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ON THE FLOW OF A COMPRESSIBLE FLUID BY THE HODOGRAPH METHOD

II—FUNDAMENTAL SET OF PARTICULAR FLOW SOLUTIONS OF THE CHAPLYGIN DIFFERENTIAL EQUATION

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SUMMARY

The differential equation of Chaplygin's jet problem is utilized to give a systematic development of particular solutions of the hodograph flow equations, which extends the treatment of Chaplygin into the supersonic range and completes the set of particular solutions.

The particular solutions serve to place on a reasonable basis the use of velocity correction formulas for the comparison of incompressible and compressible flows. It is shown that the geometric-mean type of velocity correction formula introduced in part I has significance as an over-all type of approximation in the subsonic range.

A brief review of general conditions limiting the potential flow of an adiabatic compressible fluid is given and application is made to the particular solutions, yielding conditions for the existence of singular loci in the supersonic range.

The combining of particular solutions in accordance with prescribed boundary flow conditions is not treated in the present paper.

INTRODUCTION

This paper presents a theoretical investigation that may be regarded as a continuation of studies initiated in part I (reference 1). In part I an attempt was made to unify the results of Chaplygin, von Karman and Tsien, Temple and Yarwood, and Prandtl and Glauert insofar as their results were concerned with velocity and pressure correction factors for the correspondence of incompressible and compressible flows. In addition, two new velocity correction formulas were introduced that appeared to have a somewhat wider range of applicability than the formulas of the aforementioned authors. Most of the results of part I were obtained with the use of two particular solutions of the hodograph equations. These, two basic solutions correspond to a vortex and a source in a compressible fluid.

It was mentioned in part I that, in order to treat the exact boundary problem of uniform flow of a compressible fluid past a prescribed body, a general set of particular solutions of the hodograph equations had to be obtained. Such a study is given in the present paper, which incidentally helps to clarify the nature of the velocity correction factors of part I—in particular, the one referred to as the "geometric-mean" type of approximation. In addition, many interesting types of flows are disclosed from a physical interpretation of the particular solutions. A few such solutions have already

been obtained and discussed by Ringleb (reference 2).

Several mathematical approaches exist by means of which particular integrals of the hodograph equations may be obtained. Two such approaches, mentioned in part I, may be attributed to Chaplygin (reference 3) and Bers and Gelbart (reference 4) and are analogous to an exponential and to a power-series approach, respectively. Another method of defining particular integrals is the integral-operator method of Bergman (reference 5). In the present paper the differential equation, first used by Chaplygin in his treatment of jets (reference 3), provides the basis for the definition of a complete set of particular solutions.

The scope of the present paper is limited chiefly to a systematic study of the fundamental solutions and to the physical interpretation of some of the particular flows represented by them. The combining of particular solutions to represent uniform flow past a prescribed body is not treated herein. It is believed, however, that the present study may serve as a basis for further development and clarification of this important problem.

	SYMBOLS ,
x, y	rectangular coordinates in plane of flow
q	magnitude of fluid velocity
θ	angle included by velocity vector and positive direction of x-axis
ρ	density of fluid
p	pressure in fluid
\boldsymbol{a}	velocity of sound in fluid
	Mach number (q/a)
ρ_0, p_0, a_0	quantities referred to stagnation point $q=0$
ϕ	velocity potential
ψ	stream function
γ	ratio of specific heats (approx. 1.4 for air)
$\beta = \frac{1}{\gamma - 1}$	(approx. 5/2 for air) maximum fluid velocity (corresponding to
$2\beta a_0^2$	maximum fluid velocity (corresponding to
	$p=\rho=a=0$)
τ	dimensionless speed variable
	$\left(\tau = \frac{q^2}{2\beta a_0^2} = \frac{M^2}{2\beta + M^2}\right)$
$ au_s$	sonic value of $\tau\left(\tau_{\epsilon} = \frac{1}{2\beta + 1}; \text{ approx. 1/6 for air}\right)$

For $\beta > 0$ (or $1 < \gamma < \infty$), the range of τ is $0 \le \tau \le 1$.

and

GENERAL PARTICULAR SOLUTIONS OF THE HODOGRAPH EQUATIONS

HODOGRAPH EQUATIONS

The linear equations in the hodograph variables θ and q, which relate the velocity potential ϕ and the stream function ψ for the steady two-dimensional flow of a nonviscous compressible fluid, are

$$\frac{\partial \phi}{\partial \theta} = \lambda_1(q) \frac{\partial \psi}{\partial q} \\
\frac{\partial \phi}{\partial q} = -\lambda_2(q) \frac{\partial \psi}{\partial \theta} \tag{1}$$

in which, for the adiabatic equation of state between pressure and density,

 $\lambda_1(q) = \frac{\rho_0}{2} q$

$$= \frac{q}{(1-\tau)^{\beta}}$$

$$\lambda_2(q) = -q \frac{d}{dq} \left(\frac{\rho_0}{\rho q}\right)$$

$$= \frac{\rho_0}{\rho q} (1 - M^2)$$

$$= \frac{1 - (2\beta + 1)\tau}{a(1-\tau)^{\beta+1}}$$

(See equations (21) and (25) of reference 1.)

In the incompressible case $\tau \to 0$, equations (1) can be expressed in the Cauchy-Riemann form. Particular solutions $\Omega = \phi + i\psi$ can be expressed in this case as any analytic function of the complex variable

$$w = \theta + i \log q \tag{2}$$

or as any analytic function of the related exponential function

$$e^{-iw} = qe^{-i\theta} \tag{3}$$

Thus, an infinite set of particular integrals of equations (1), in the incompressible case, referred to herein as "the powers set," is w^k . When k is a positive integer, the particular solutions vanish at the origin $(\theta=0, \log q=0)$ and, when k is a negative integer, the particular solutions are infinite at the origin. In the case of nonintegral values of k, the origin is a branch point of the functions w^k .

Another infinite set of particular integrals of equations (1) in the incompressible case, referred to herein as "the exponential set," is

$$(e^{-iw})^k = q^k e^{-ik\theta}$$

where, again, k can take on any value—integral, nonintegral, positive, or negative.

In the compressible case, the particular solutions corresponding to the powers set w^{t} (that is, the particular solutions which reduce to w^{t} in the incompressible case $\tau \rightarrow 0$) depend on whether the coefficient of w^{t} is real or imaginary—a consequence of the fact that, in the compressible case, ϕ and ψ do not satisfy the same differential equation. For

example, for k=1, the two functions corresponding to w and iw, which have been developed in part I, are

$$W= heta+iL$$
 and $i ilde{W}=i(heta+i ilde{L})$ where $L=\log q+f(au)$ and $ilde{L}=\log q+q(au)$

and $f(\tau)$ and $g(\tau)$ each vanish for $\tau=0$. (See equations (26) and (27) of reference 1.)

The development of other functions corresponding to the power set w^k , for positive integral values of k, follows according to the method of Bers and Gelbart. (See expression (22) of reference 1.) Since the present paper is chiefly concerned with the functions corresponding to the exponential set e^{-ikv} , the powers set is not further discussed.

CHAPLYGIN DIFFERENTIAL EQUATION

THE FUNCTIONS PL AND QL

Corresponding to the exponential sets in the incompressible case

$$e^{-i\mathbf{k}\mathbf{v}} = q^{\mathbf{k}} \cos k\theta - iq^{\mathbf{k}} \sin k\theta$$

and

$$ie^{-ikw} = q^k \sin k\theta + iq^k \cos k\theta$$

there appear in the compressible case functions designated, respectively,

$$P_{k}(q) \cos k\theta - iQ_{k}(q) \sin k\theta$$

and

$$P_{k}(q) \sin k\theta + iQ_{k}(q) \cos k\theta$$

where the functions $P_{k}(q)$ and $Q_{k}(q)$ satisfy second-order differential equations. These equations are easily obtained by substituting in equations (1) the product-type solutions

$$\phi_{k} = P_{k}(q) \begin{cases} \cos (k\theta) \\ \sin (k\theta) \end{cases}$$

$$\psi_{k} = Q_{k}(q) \begin{cases} \sin (-k\theta) \\ \cos (k\theta) \end{cases}$$
(4)

In view of equations (1) it is observed that

$$kP_{k}(q) = \frac{\rho_{0}}{\rho} q \frac{dQ_{k}(q)}{dq}$$

$$\frac{dP_{k}(q)}{dq} = -kq \frac{d}{dq} \left(\frac{\rho_{0}}{\rho q}\right) Q_{k}(q)$$
(5)

The functions $Q_k(q)$ satisfy the second-order differential equation

$$q^{2} \frac{d^{2}Q_{k}}{dq^{2}} + (1 + M^{2})q \frac{dQ_{k}}{dq} - k^{2}(1 - M^{2})Q_{k} = 0$$
 (6)

The functions $P_{k}(q)$ can be obtained from $Q_{k}(q)$ by means of the first of equations (5). Equation (6) may be reduced to a standard type by introducing τ as the independent variable. Put

$$Q_{\mathbf{k}}(q) = q^{\mathbf{k}} Y_{\mathbf{k}}(\tau) \tag{7}$$

where clearly $Y_k(\tau) \rightarrow 1$ as $\tau \rightarrow 0$ (incompressible case). With the use of the symbolic relations

$$q \frac{d}{dq} = 2\tau \frac{d}{d\tau}$$

$$q^2 \frac{d^2}{dq^2} = 4\tau^2 \frac{d^2}{d\tau^2} + 2\tau \frac{d}{d\tau}$$

and the relation

$$M^2 = \frac{2\beta\tau}{1-\tau}$$

the desired differential equation is

$$\tau(1-\tau)\frac{d^{2}Y_{k}}{d\tau^{2}} + [(k+1) - (k+1-\beta)\tau]\frac{dY_{k}}{d\tau} + \frac{1}{2}\beta k(k+1)Y_{k} = 0$$
(8)

Equation (8), which is of the hypergeometric type, was first introduced by Chaplygin in his memoir on gas jets (reference 3).

THE FUNCTIONS Y's AND Y-1

Chaplygin treated the subsonic flow of a compressible fluid through jets with straight-line boundaries. For such problems the hodograph variables θ and q are natural variables in the sense that the solid and fluid boundaries are described by θ =Constant and q=Constant, respectively, and only the particular solutions of equation (8) with positive characteristic index k are needed. In the present paper a complete ordered set of particular solutions of equation (8) is obtained, which extends the results of Chaplygin into the supersonic range and to negative values of the index k. Two types of solutions of equation (8) for nonintegral values of k are

 $Y_{\mathbf{k}}(\tau) = F(a_{\mathbf{k}}, b_{\mathbf{k}}, k+1; \tau) \tag{9}$

and

 $\overline{Y}_{k}(\tau) = \tau^{-k} F(a_{k} - k, b_{k} - k, 1 - k; \tau)$ (10)

where

 $a_k + b_k = k - \beta$

 $a_k b_k = -\frac{k}{2} (k+1) \beta$

and

$$F(a, b, c; \tau) = 1 + \frac{ab}{c}\tau + \frac{a(a+1)b(b+1)}{2!}\tau^2 + \dots$$

It is now shown that only one of the solutions need be used. For positive values of k, the requirement that $Y_k(0)=1$ excludes the use of equation (10). For negative values of the index, the solution $\overline{Q}_{-k}(q)=q^{-k}\overline{Y}_{-k}(\tau)$ obtained with the aid of equation (10) is, except for a constant factor, equivalent to the solution $Q_k(q)=q^kY_k(\tau)$ obtained with the aid of equation (9). Thus

$$\begin{split} \overline{Q}_{-k}(q) &= q^{-k} \overline{Y}_{-k}(\tau) \\ &= q^{-k} \tau^{k} F(a_{-k} + k, b_{-k} + k, k + 1; \tau) \\ &= q^{-k} \tau^{k} F(a_{k}, b_{k}, k + 1; \tau) \\ &= \left(\frac{1}{2\beta a_{0}^{2}}\right)^{k} Q_{k}(q) \end{split}$$

Hence, only the solutions given by equation (9) are needed for the determination of $Q_{k}(q)$ and $Q_{-k}(q)$. Then

 $Q_{k}(q) = q^{k} Y_{k}(\tau)$ $= q^{k} F(a_{k}, b_{k}, k+1; \tau)$ (11)

and

$$Q_{-k}(q) = q^{-k} Y_{-k}(\tau)$$

$$= q^{-k} F(a_{-k}, b_{-k}, -k+1; \tau)$$

$$= q^{-k} F(a_{k}-k, b_{k}-k, -k+1; \tau)$$
(12)

Observe that both types of hypergeometric functions appearing in equations (9) and (10) are utilized in the expressions for $Q_k(q)$ and $Q_{-k}(q)$.

The foregoing discussion has been limited to nonintegral values of the index, positive or negative. When the index is integral and positive, equations (9) and (11) remain valid. When the index is integral and negative, however, equation (12) does not in general lead to a meaningful solution and consequently another independent solution is to be sought. The desired solution for $Y_{-k}(\tau)$ in such cases contains a logarithmic term and again is subject to the condition that it reduce to unity for $\tau=0$ (incompressible case). The expression for $Q_{-k}(q)$ is then given by

$$Q_{-k}(q) = q^{-k} Y_{-k}(\tau) \tag{13}$$

where

and

$$\begin{split} Y_{-k}(\tau) &= 1 - \frac{(a_k - k)(b_k - k)}{1!(k-1)} \tau + \frac{(a_k - k)(a_k - k + 1)(b_k - k)(b_k - k + 1)}{2!(k-1)(k-2)} \tau^2 \\ &- \frac{(a_k - k)(a_k - k + 1)(a_k - k + 2)(b_k - k)(b_k - k + 1)(b_k - k + 2)}{3!(k-1)(k-2)(k-3)} \tau^3 + \dots \\ &+ (-1)^{k-1} \frac{(a_k - k)(a_k - k + 1) \dots (a_k - 2)(b_k - k)(b_k - k + 1) \dots (b_k - 2)}{(k-1)!(k-1)!} \tau^{k-1} \\ &+ c \left[\tau^k F(a_k, b_k, k + 1; \tau) \log \tau + \frac{a_k b_k}{1!(k+1)} \left(\frac{1}{a_k} + \frac{1}{b_k} - \frac{1}{1} - \frac{1}{k+1} \right) \tau^{k+1} \right. \\ &+ \frac{a_k (a_k + 1)b_k (b_k + 1)}{2!(k+1)(k+2)} \left(\frac{1}{a_k} + \frac{1}{a_k + 1} + \frac{1}{b_k} + \frac{1}{b_k + 1} - \frac{1}{1} - \frac{1}{2} - \frac{1}{k+1} - \frac{1}{k+2} \right) \tau^{k+2} + \dots \right] \\ c &= (-1)^{k+1} \frac{(a_k - 1)(a_k - 2) \dots (a_k - k)(b_k - 1)(b_k - 2) \dots (b_k - k)}{k!(k-1)!} \end{split}$$

Note that, if a_k or b_k takes on any of the values 1, 2, . . . k, the constant c equals zero and the function $Y_{-k}(\tau)$ becomes a polynomial. It should be pointed out, however, that equation (13) is to be utilized only if equation (12) does not yield a relevant and finite result. This statement is illustrated in some of the following special examples.

Case of $\gamma = -1$:

Consider as an example the von Kármán-Tsien treatment of compressible flow (reference 6) in which the adiabatic index $\gamma = -1$ or $\beta = -\frac{1}{2}$. Then

$$a_{k} = \frac{k+1}{2}$$

$$b_{k} = \frac{k}{2}$$

For a negative integral index, equation (13) may appear to be applicable, in which case the expression for $Y_{-k}(\tau)$ would be a polynomial of degree k-1. An examination of equation (12) shows, however, that for this case no infinities arise and that, when the index is negative, integral, or nonintegral,

$$Y_{-k}(\tau) = F\left(\frac{1-k}{2}, -\frac{k}{2}, 1-k; \tau\right)$$

The hypergeometric series represented by $Y_{-k}(\tau)$ converges for values $0 \le |\tau| < 1$. For the present case of $\gamma = -1$ or $\beta = -\frac{1}{2}$, values of τ corresponding to positive values of M lie outside the range of convergence. A closed expression for $Y_{-k}(\tau)$ can be found, however, for this case which, by analytic continuation, is therefore valid for all values of τ . Thus

$$Y_{-k}(\tau) = F\left(\frac{1-k}{2}, -\frac{k}{2}, 1-k; \tau\right)$$
$$= \left\lceil \frac{1+(1-\tau)^{1/2}}{2} \right\rceil^{k}$$

Similarly, from equation (9), when the index is positive,

$$Y_{k}(\tau) = F\left(\frac{1+k}{2}, \frac{k}{2}, 1+k; \tau\right)$$

$$= \left[\frac{1+(1-\tau)^{1/2}}{2}\right]^{-k}$$

Observe that

$$Q_{k}(q) = \frac{1}{Q_{-k}(q)} \qquad \qquad 0$$

$$= \left[q \frac{2}{1 + (1 - \tau)^{1/2}} \right]^{k} \qquad (14)$$

This identity for the von Kármán-Tsien case corresponds to the identity $q^{k} = \frac{1}{q^{-k}}$ for the incompressible case.

Case of k=1:

For k=1,

$$a_1 = 1$$
 $b_1 = -\beta$ $c_1 = 2$

Then, for the positive index,

$$Q_{1}(q) = qY_{1}(\tau)$$

$$= qF(1, -\beta, 2; \tau)$$

$$= q\frac{1 - (1 - \tau)^{\beta + 1}}{(\beta + 1)\tau}$$
(15)

For the negative integral index, it may appear at first glance that equation (13) is needed; however, equation (12) does yield a relevant and finite result and accordingly is the equation to be used. Thus

$$\lim_{k \to 1} F(a_k - k, b_k - k, 1 - k; \tau) = 1 + \frac{\beta}{2} \tau - \frac{\beta^2}{2 \times 2!} \tau^3 + \frac{\beta^2 (\beta - 1)}{2 \times 3!} \tau^3 - \frac{\beta^2 (\beta - 1) (\beta - 2)}{2 \times 4!} \tau^4 + \dots$$

$$= 1 + \frac{1}{2} \frac{\beta}{\beta + 1} \left[1 - (1 - \tau)^{\beta + 1} \right]$$

and therefore

$$Q_{-1}(\tau) = q^{-1} \left\{ 1 + \frac{1}{2} \frac{\beta}{\beta + 1} \left[1 - (1 - \tau)^{\beta + 1} \right] \right\}$$
 (16)

Case of k=0:

The exceptional case of k=0 is directly treated by means of equation (8). The differential equation for $Y_0(\tau)$ or $Q_0(\tau)$ then is

$$\frac{d}{d\tau} \left[\frac{\tau}{(1-\tau)^{\beta}} \frac{dQ_0}{d\tau} \right] = 0$$

The general solution of this equation can be written as

$$Q_0(q) = 2C_1 \log q + C_1 \int_0^{\tau} [(1-\tau)^{\beta} - 1] \frac{d\tau}{\tau} + C_2$$

where C_1 and C_2 are arbitrary constants of integration. The constants C_1 and C_2 are determined by the imposed condition that the expression for $Q_0(q)$ reduce in the incompressible case simply to $\log q$. Then

$$C_1 = \frac{1}{2}$$

 $C_0 = 0$

and therefore

$$Q_0(q) = \log q + \frac{1}{2} \int_0^{\tau} [(1-\tau)^{\beta} - 1] \frac{d\tau}{\tau}$$
 (17)

In a similar manner, from the differential equation for P_0 ,

$$\frac{d}{d\tau} \left[\frac{\tau(1-\tau)^{\beta+1}}{1-(2\beta+1)\tau} \frac{dP_0}{d\tau} \right] \! = \! 0$$

the expression for P_0 is obtained as

$$P_0(q) = \log q + \frac{1}{2} \int_0^{\tau} \left[\frac{1 - (2\beta + 1)\tau}{(1 - \tau)^{\beta + 1}} - 1 \right] \frac{d\tau}{\tau}$$
 (18)

It is remarked that the functions $Q_0(q)$ and $P_0(q)$ are identical with the elementary functions L(q) and $\tilde{L}(q)$, respectively, introduced in part I (reference 1) and are associated with a vortex and a source type of flow.

THE FUNCTIONS R. AND S.

A linear homogeneous differential equation of order ncan, in general, be reduced to a differential equation of order n-1 by means of an exponential-type substitution for the dependent variable. Chaplygin made use of such a substitution to reduce the second-order differential equations satisfied by P_k and Q_k to first-order equations of the Riccati form, in order to study properties of the functions P_k and Q_k in the subsonic range for only positive values of k. In the present analysis the Riccati equations are also found useful in order to extend the study of the functions P_{k} and Q_{k} to the supersonic range for both positive and negative values of the

The second-order differential equations for P_{k} and Q_{k} , with τ as the independent variable, are

$$\frac{d}{d\tau} \left\lceil \frac{\tau (1-\tau)^{\beta+1}}{1-(2\beta+1)\tau} \frac{dP_{\mathbf{k}}}{d\tau} \right\rceil - \frac{k^2}{4} \frac{(1-\tau)^{\beta}}{\tau} P_{\mathbf{k}} = 0$$

and

$$\frac{d}{d\tau} \left[\frac{\tau}{(1-\tau)^{\beta}} \frac{dQ_k}{d\tau} \right] - \frac{k^2}{4} \frac{1-(2\beta+1)\tau}{\tau(1-\tau)^{\beta+1}} Q_k = 0$$

The corresponding first-order Riccati equations are obtained by substituting for P_k and Q_k new dependent variables R_k and S_k , respectively, as follows:

or
$$P_{\mathbf{k}} = e^{\int \frac{\mathbf{k}}{2\tau} R_{\mathbf{k}} d\tau}$$

$$R_{\mathbf{k}} = \frac{2\tau}{k} \frac{1}{P_{\mathbf{k}}} \frac{dP_{\mathbf{k}}}{d\tau}$$

$$= \frac{2\tau}{k} \frac{d}{d\tau} \log P_{\mathbf{k}}$$
and (19)

$$Q_{\mathbf{k}} = e^{\int \frac{\mathbf{k}}{2\tau} S_{\mathbf{k}} d\tau}$$

or

$$S_{\mathbf{k}} = \frac{2\tau}{k} \frac{1}{Q_{\mathbf{k}}} \frac{dQ_{\mathbf{k}}}{d\tau}$$

$$= \frac{2\tau}{k} \frac{d}{d\tau} \log Q_k \tag{20}$$

The equations satisfied by $R_{k}(\tau)$ and $S_{k}(\tau)$ are

$$\frac{dR_{k}}{d\tau} + \frac{1 + (2\beta + 1)\tau}{1 - (2\beta + 1)\tau} \frac{\beta}{1 - \tau} R_{k} + \frac{k}{2\tau} \left[R_{k}^{2} - \frac{1 - (2\beta + 1)\tau}{1 - \tau} \right] = 0 \quad (21)$$

and

$$\frac{dS_{k}}{d\tau} + \frac{\beta}{1-\tau} S_{k} + \frac{k}{2\tau} \left[S_{k}^{2} - \frac{1 - (2\beta + 1)\tau}{1-\tau} \right] = 0$$
 (22)

Initial conditions for $R_k(\tau)$ and $S_k(\tau)$ are found by examination of the incompressible case $\tau \to 0$. $P_k = Q_k = q^k$ and, since $2\tau \frac{d}{d\tau} = q \frac{d}{dq}$, it follows from equations (19) and (20) that

$$R_{k}(0) = S_{k}(0) = 1$$

The following important relation exists between the functions $R_{\mathbf{k}}(\tau)$ and $S_{\mathbf{k}}(\tau)$:

$$R_{k}(\tau)S_{k}(\tau) = \frac{1 - (2\beta + 1)\tau}{1 - \tau}$$

$$= 1 - M^{2}$$
(23)

Equation (23) can be verified directly from the hodograph equations (1). It may be noted at this point that this result is of significance in connection with the geometric-mean type of velocity correction factor introduced in part I and is discussed more fully in a later section.

Before the functions $R_k(\tau)$ and $S_k(\tau)$ are treated, certain general observations can be made regarding the functions $P_{k}(\tau)$, $Q_{k}(\tau)$, $R_{k}(\tau)$, and $S_{k}(\tau)$. Chaplygin, who limited his investigations to the subsonic range and to positive values of the index k, has shown that Q_k and consequently the other functions possess no roots for any value of the independent variable in the subsonic range, with M=0 excluded. In the supersonic range M>1, $P_k(\tau)$ and $Q_k(\tau)$ in general possess zeros. Certain relations obtained by means of equations (19), (20), and (23) between P_k , Q_k , R_k , and S_k at the zeros of P_k and Q_k are summarized as follows:

Pk	Qa	$\frac{dP_k}{d\tau}$	dQk dr	R	Sk
0	Max or min		0	80	0
Max or min	0	0		0	80

It is remarked that the number of zeros of Q_{k} , as a function of the index k, can be found from an expression developed by Klein and Hurwitz (reference 7) in connection with the zeros of the hypergeometric function. In general, the number of zeros increases with the magnitude of the index kand is infinite for $k=\pm\infty$.

A further observation of interest can be made in connection with equation (23). Chaplygin has shown that, for positive finite values of k (and the same is true for negative finite values of k), the functions $S_k(\tau)$ are not zero for the sonic value $\tau = \tau_*$ or M=1. From equation (23) then, it follows that the functions $R_k(\tau)=0$ for M=1.

In view of the relation between the functions R_{k} and S_{k} given by equation (23), only S_k need be discussed. The Riccati equation (22) may be used to discuss certain properties of the function S_k but in general, for numerical evaluation, the original definition (equation (20)) in terms of the function Q_k may be used directly:

$$S_k = \frac{2\tau}{k} \frac{1}{Q_k} \frac{dQ_k}{d\tau}$$

or

$$S_{\mathbf{k}} = 1 + \frac{2\tau}{Y_{\mathbf{k}}} \frac{dY_{\mathbf{k}}}{d\tau}$$

In general, the functions S_{k} are expressible in infinite series. For several values of k, however, S_k can be expressed in closed forms. For k=0 and $k=\pm\infty$, S_k may be obtained by a limiting process from equation (20); however, for these special cases the Riccati equation (equation (22)) yields the results directly. Thus

 $S_0 = (1 - \tau)^{\beta} \tag{24}$

and

$$S_{-\infty} = \left[\frac{1 - (2\beta + 1)\tau}{1 - \tau} \right]^{1/2}$$
$$= (1 - M^2)^{1/2}$$
 (25)

The cases k=1 and k=-1 may also be expressed in closed form. With the aid of the equations (15) and (16) for Q_1 and Q_{-1} , equation (20) yields

$$S_1 = 1 - 2 \frac{1 - (1 + \beta \tau)(1 - \tau)}{1 - (1 - \tau)^{\beta + 1}}$$
 (26)

and

$$S_{-1} = 1 - \frac{\beta \tau (1 - \tau)^{\beta}}{1 + \frac{1}{2} \frac{\beta}{\beta + 1} \left[1 - (1 - \tau)^{\beta + 1} \right]}$$
(27)

In order to illustrate the behavior of some of the functions thus far introduced, a number of tables and figures are given. All the calculations have been performed with the adiabatic index $\gamma=1.4$. Table 1 gives values of Y_k as a function of M or τ for several positive and negative values of the index k. Figure 1 shows the functions Y_k plotted against M. Values of the functions S_k and R_k are given in tables 2 and 3 and are plotted against M in figures 2 and 3.

THE FUNCTIONS $f_k(\tau)$ AND $g_k(\tau)$

In the incompressible case, the sets of functions Q_k and P_k can be reduced to a single function $\log q$ by means of a simple operator $\frac{1}{k} \log$. Thus

 $Q_{k}=P_{k}=q^{k}$

and

$$\frac{1}{k}\log q^k = \log q$$

This same operation applied to the functions Q_k and P_k in the compressible case serves to define two useful sets of functions $\log q + f_k(\tau)$ and $\log q + g_k(\tau)$, respectively. Thus

 $\frac{1}{L}\log Q_{k} = \log q + f_{k}(\tau) \tag{28}$

and

$$\frac{1}{k}\log P_{k} = \log q + g_{k}(\tau) \tag{29}$$

From equation (7), namely,

 $Q_{\mathbf{k}} = q^{\mathbf{k}} Y_{\mathbf{k}}(\tau)$

it follows that

$$f_{k}(\tau) = \frac{1}{k} \log Y_{k}(\tau) \tag{30}$$

From equation (5) for P_k and equation (20), which defines S_k ,

$$P_{\mathbf{k}} = \frac{1}{(1-\tau)^{\beta}} Q_{\mathbf{k}} S_{\mathbf{k}}$$

It follows that

$$g_{k}(\tau) = \frac{1}{k} \log \frac{Y_{k}(\tau)S_{k}(\tau)}{(1-\tau)^{\beta}}$$

$$= f_{k}(\tau) + \frac{1}{k} \log \frac{S_{k}}{(1-\tau)^{\beta}}$$
(31)

For example, for k=1 and k=-1 and with the use of equations (15) and (16),

$$f_1(\tau) = \log \frac{1 - (1 - \tau)^{\beta + 1}}{(\beta + 1)\tau}$$
 (32)

$$g_1(\tau) = \log \frac{(1-\tau)^{\beta} [1+(2\beta+1)\tau] - 1}{(\beta+1)\tau(1-\tau)^{\beta}}$$
(33)

$$f_{-1}(\tau) = -\log\left\{1 + \frac{1}{2}\frac{\beta}{\beta + 1}\left[1 - (1 - \tau)^{\beta + 1}\right]\right\}$$
 (34)

$$g_{-1}(\tau) = -\log \frac{(3\beta + 1) - \beta(1+\tau)(1-\tau)^{\beta}}{2(\beta + 1)(1-\tau)^{\beta}}$$
(35)

For k=0 and $k=\pm\infty$, equations (30) and (31) require a limiting process for their evaluation. Alternate forms for $f_k(\tau)$ and $g_k(\tau)$ may be obtained, however, by means of equations (19) and (20) defining $R_k(\tau)$ and $S_k(\tau)$, which yield the results for k=0 and $k=\pm\infty$ directly. Thus

 $f_{k}(\tau) = \frac{1}{2} \int_{0}^{\tau} [S_{k}(\tau) - 1] \frac{d\tau}{\tau}$ (36)

and

$$g_{k}(\tau) = \frac{1}{2} \int_{0}^{\tau} [R_{k}(\tau) - 1] \frac{d\tau}{\tau}$$
 (37)

where $R_k(\tau)$ and $S_k(\tau)$ are related according to equation (23). Then

$$f_0(\tau) = \frac{1}{2} \int_0^{\tau} [(1 - \tau)^{\beta} - 1] \frac{d\tau}{\tau}$$
 (38)

$$g_0(\tau) = \frac{1}{2} \int_0^{\tau} \left[\frac{1 - (2\beta + 1)\tau}{(1 - \tau)^{\beta + 1}} - 1 \right] \frac{d\tau}{\tau}$$
 (39)

and

$$f_{+\infty}(\tau) = g_{+\infty}(\tau) = \frac{1}{2} \int_0^{\tau} \left\{ \left[\frac{1 - (2\beta + 1)\tau}{1 - \tau} \right]^{1/2} - 1 \right\} \frac{d\tau}{\tau} \quad (40)$$

It is worthy of special notice that the functions $f_0(\tau)$, $g_0(\tau)$, and $f_{-\infty}(\tau)$ are identical with the functions $f(\tau)$, $g(\tau)$, and $h(\tau)$, respectively, which formed the basis of part I (reference 1). In addition, the expressions $\log q + f_0(\tau)$, $\log q + g_0(\tau)$, and $\log q + f_{-\infty}(\tau)$ are identical with the functions L, L and H, respectively, which were introduced in part I.

A number of functions f_k and g_k have been calculated, with $\gamma=1.4$, for several positive and negative values of the index k, and the values are given in tables 4 and 5 and plotted in figures 4 and 5.

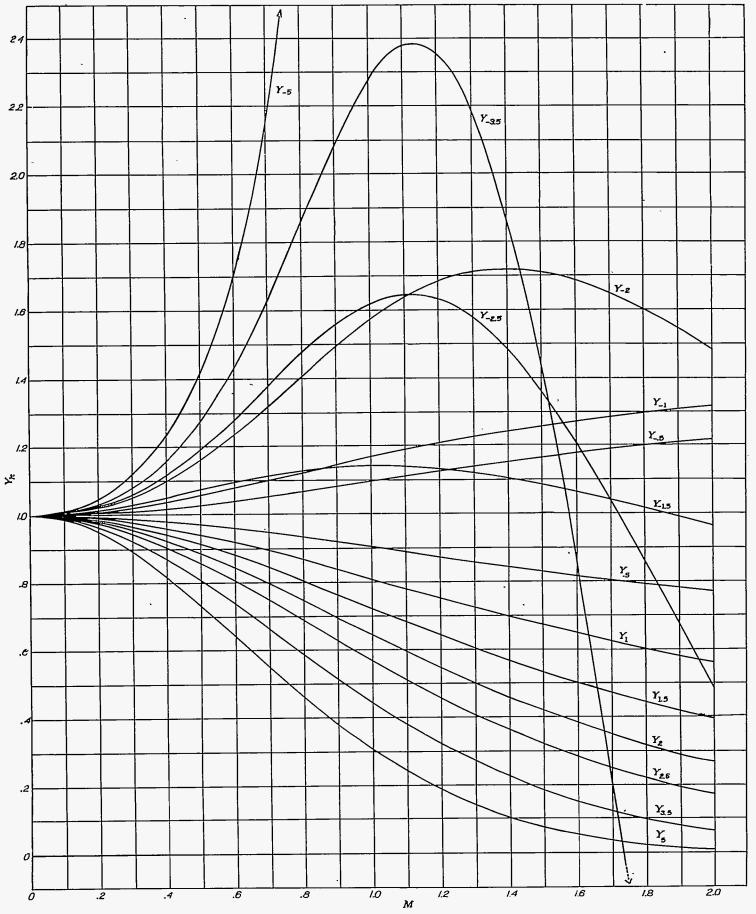


FIGURE 1.—The functions Y_k against M for several values of the index k.

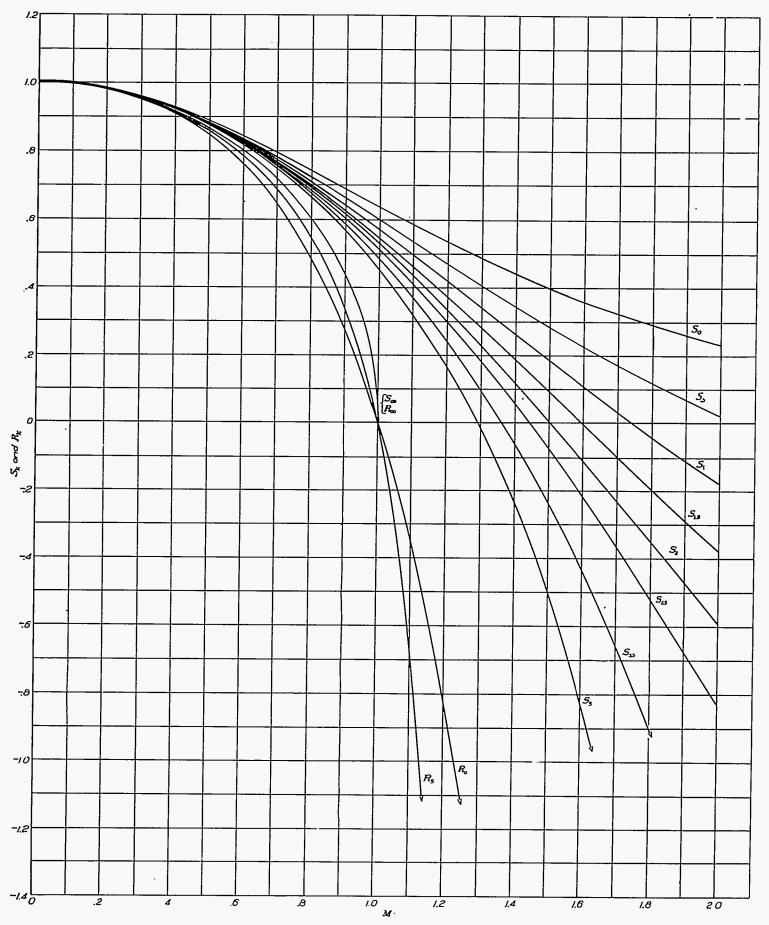


Figure 2.—The functions S_k and R_k against M for several positive values of the index k.

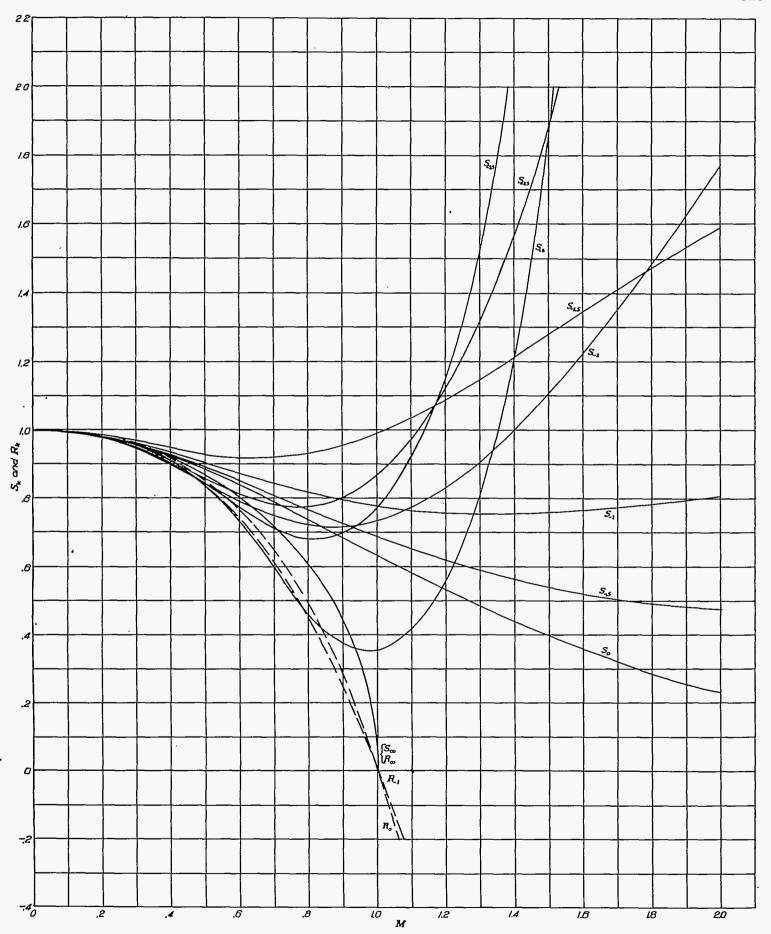


FIGURE 8.—The functions S_k and R_k against M for several negative values of the index k.

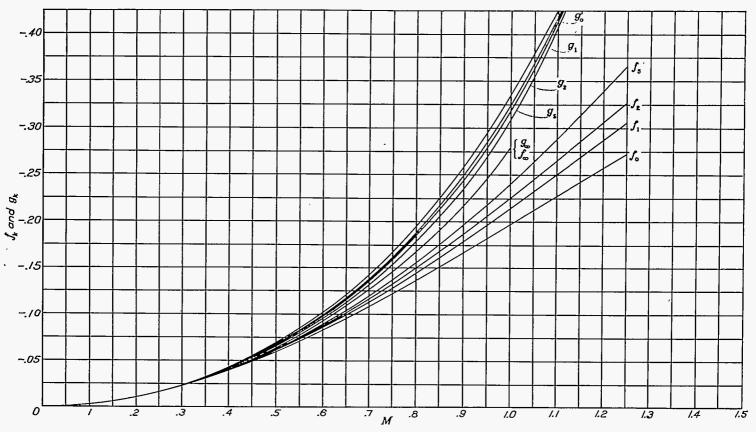


Figure 4.—The functions f_k and g_k against M for several positive values of the index k.

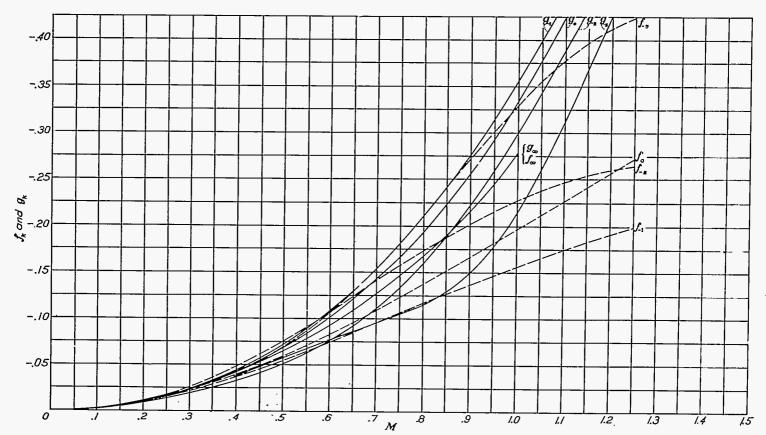


Figure 5.—The functions f_k and g_k against M for several negative values of the index k.

The opportunity is taken here to note that, for the von Karman-Tsien case $\left(\gamma = -1 \text{ or } \beta = -\frac{1}{2}\right)$,

$$\begin{aligned} f_{k} &= g_{k} = -\log \frac{1 + (1 - \tau)^{1/2}}{2} \\ &= \log \frac{2\sqrt{1 - M^{2}}}{1 + \sqrt{1 - M^{2}}} \end{aligned}$$

and that the sets of functions P_k and Q_k , as in the incompressible case, are reduced to a single function by the operator $\frac{1}{k}$ log; namely (compare equation (14)),

$$\log q + \log \frac{2\sqrt{1-M^2}}{1+\sqrt{1-M^2}}$$

In fact, the complex flow potential $\phi + i\psi$ can be expressed as an analytic function of a single complex variable $\theta + i \log q \frac{2\sqrt{1-M^2}}{1+\sqrt{1-M^2}}$. Tsien has made use of this complex variable in his hodograph treatment of the compressible flow past an elliptic cylinder (reference 8).

VELOCITY CORRECTION FACTOR

The solution of the problem of an exact correspondence between the flow past a prescribed body in an incompressible fluid and the flow past the same body in a compressible fluid is a difficult matter. This problem can be solved exactly for certain types of flow patterns (not past closed shapes), such as flows inside or outside angles or channels, and for certain flow singularities such as a vortex, source, and doublet-types of flow which can be associated with the particular solutions Q_k . Some of these types of flow are illustrated by examples in the following section. Combining particular solutions to represent uniform flow past a prescribed body is a complicated process, since the treatment of infinite series in the functions Q_{κ} for both positive and negative values of k is involved. Furthermore, the process of returning to the physical-plane variables from the hodograph-plane variables hinges on nonelementary parts of differential geometry. Certain types of jet problems can be properly treated in the subsonic range by series in Q_k with k positive, as was shown by Chaplygin (reference 3). Thus, it appears that much work remains to be done in order to render feasible exact and practical solutions for uniform flow past prescribed bodies in a compressible fluid. Because of the difficulty and complexity of the general problem of flow in a compressible fluid, attempts have been made by a number of investigators to obtain results by means of velocity correction formulas that serve to place in correspondence velocities in an incompressible and in a compressible

In part I the velocity correction factor was discussed with particular reference to the two functions L and \tilde{L} (Q_0 and P_0 of the present paper) associated with a vortex and source type of flow, respectively. The main justification for the results of part I was the yielding and the unifying of the results of Chaplygin, von Karman and Tsien, Temple and

Yarwood, and Prandtl and Glauert. The knowledge of the infinite set of functions P_k and Q_k discussed in the present paper can now serve to establish further on a reasonable basis the concept of a velocity correction formula.

In order that a single velocity correction factor be feasible, even for a flow associated with a particular solution, it is necessary that $P_k \approx Q_k$. Consider, for example, the functions Q_k and P_k insofar as the first power of the variable τ is concerned. It can be shown easily that

$$\frac{1}{k} \log Q_{k} = \log q + f_{k}(\tau)$$

$$\approx \log q - \frac{1}{2}\beta\tau$$

and

$$\frac{1}{k}\log P_{k} = \log q + g_{k}(\tau)$$

$$\approx \log q - \frac{1}{2} \beta \tau$$

Thus, to the first power of τ and independent of k,

$$f_{k}(\tau) = g_{k}(\tau)$$

$$\approx -\frac{1}{2} \beta \tau$$

$$P_{k} \approx Q_{k}$$

Then

or

$$_{\mathbf{k}}pprox Q_{\mathbf{k}}$$
 $pprox \left(qe^{-rac{1}{2}eta_{r}}
ight)^{\mathbf{k}}$

The nature of the correspondence between the incompressible flow and the compressible flow is such that

Without going into any details here of the field point correspondence or of the boundary distortion, the velocities in the incompressible and compressible cases may be placed in correspondence as follows:

 $(\log q)_{i} = \left(\log q - \frac{1}{2} \beta \tau\right)_{e}$ $q_{i} = q_{e} e^{-\frac{1}{2} \beta \tau} \tag{42}$

This result implies that the complex variable

$$\theta + i \left(\log q - \frac{1}{2} \beta \tau \right)$$

in the compressible case corresponds to the complex variable $\theta+i$ log q in the incompressible case. Equation (42) represents the approximation of Temple and Yarwood discussed in part I.

Consider now the functions Q_k and P_k insofar as large values of the index k are concerned. It is recalled that, as the index $k \to \pm \infty$,

$$R_{k} \rightarrow S_{k}$$

$$\rightarrow (1 - M^{2})^{1/2}$$

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and that

$$\frac{1}{k}\log Q_{k} \rightarrow \frac{1}{k}\log P_{k}$$

$$\rightarrow \log q + h(\tau)$$

where

$$h(\tau) = f_{-\infty}(\tau) = g_{-\infty}(\tau)$$

Then, as $k \to \pm \infty$,

$$P_{\mathbf{k}} \approx Q_{\mathbf{k}}$$

$$\approx [qe^{h(\mathbf{r})}]^{\mathbf{k}}$$

The function $h(\tau)$ is expressed in integral form in equation (40) and has been evaluated and tabulated in part I. (See also table 4 and fig. 4 of the present paper.) The correspondence of velocities in the incompressible and the compressible case is given by

$$q_i = q_c e^{h(\tau)} \tag{43}$$

Equation (43) constitutes the geometric-mean velocity correction formula introduced in part I and is limited to the subsonic range $0 \le M \le 1$. It is observed that, for positive values of k, $h(\tau)$ lies between $f_k(\tau)$ and $g_k(\tau)$ in magnitude. Moreover, the deviation of $e^{h(\tau)}$ from $e^{f_k(\tau)}$ and $e^{g_k(\tau)}$ is quite small in the subsonic range. (See table 6.)

The foregoing remarks, together with the fact that the geometric-mean type of approximation contains the results of Chaplygin, von Karman and Tsien, Temple and Yarwood, and in the limiting case of small disturbances to the main flow the exact Prandtl-Glauert rule, lead to the suggestion that it may be adopted as an over-all type of approximation in the subsonic range.

FLOW PATTERNS CORRESPONDING TO THE PARTICULAR SOLUTIONS

Before the flow patterns corresponding to the particular solutions ϕ_k and ψ_k given by equations (4) for the compressible case are discussed, it is instructive to examine the incompressible case. Consider the complex velocity potential

$$\Omega = \phi + i\psi \\
= Uz^n \tag{44}$$

where U and n are constants and z=x+iy. It is well known that, if $n=\frac{\pi}{\alpha}$ where α is an angle between 0 and 2π , equation (44) represents the flow in a sharp angle. For example, the flow inside a right angle is obtained with n=2 and the flow outside a right angle is obtained with $n=\frac{2}{3}$. Again, the value n=1 or $\alpha=\pi$ corresponds to a uniform flow and the value $n=\frac{1}{2}$ or $\alpha=2\pi$ corresponds to the flow around a semi-infinite line. Clearly, all the angle flows are obtained with values of n between $\frac{1}{2}$ and ∞ . Other types of flows are given by other values of n. For example, n=-1 corresponds to a doublet and the remaining negative integers are associated with singularities of higher order than the doublet. In addition to the flows described by the powers z^n , there are

the two fundamental flows, the source and the vortex, associated with the function $\log z$. If, now, it is desired to obtain generalizations for the compressible case of the foregoing particular flows, the procedure is first to express ϕ or ψ for the incompressible flow as a function of the hodograph variables q and θ and then to replace q^* by P_k or Q_k , respectively. Several examples will best illustrate this procedure:

(1) Consider the compressible generalization of the angle flows. By means of the relation

$$\frac{d\Omega}{dz} = e^{-iw}$$

where $w=\theta+i\log q$, the hodograph complex variable w is introduced as independent variable in place of z. From equation (44)

$$\frac{d\Omega}{dz} = nUz^{n-1}$$

$$= e^{-iw}$$

Hence

$$z = \frac{1}{(Un)^{\frac{1}{n-1}}} (e^{-iw})^{\frac{1}{n-1}}$$

and

$$\Omega = \frac{U}{(Un)^{\frac{n}{n-1}}} (e^{-tw})^{\frac{n}{n-1}}$$

Then

$$\psi = -\frac{U}{(U_n)^{\frac{n}{n-1}}} q^{\frac{n}{n-1}} \sin \frac{n}{n-1} \theta$$

If $\frac{n}{n-1}$ is replaced by k, the compressible generalization of the angle flows is given by

$$\psi_{\mathbf{k}} = -\frac{U}{\left(U_{\overline{k}-1}\right)^{\mathbf{k}}} Q_{\mathbf{k}} \sin k\theta \tag{45}$$

The inside angle flows are given by values of k in the range $1 < k < \infty$ and the outside angle flows, by values of k in the range $1 \le -k < \infty$. For example, k=2 for the flow inside a right angle, and k=-2 for the flow outside a right angle. Other types of flow are given by values of k in the range $-1 < k \le 1$.

The case k=1 or $n=\pm\infty$ is exceptional and, in fact, corresponds to the incompressible flow

$$\Omega = e^{cs} \tag{46}$$

where c is a constant.

(2) Consider the compressible generalization of the doublet. The complex velocity potential for the incompressible doublet at the origin is

$$\Omega = \frac{1}{2}$$

The reflected-velocity vector is

$$\frac{d\Omega}{dz} = -\frac{1}{z^2}$$

Hence

$$z=ie^{\frac{1}{2}iw}$$

and

$$\Omega = -ie^{-\frac{1}{2}iw}$$

The stream function for the incompressible doublet is then given by

$$\psi = -q^{\frac{1}{2}}\cos\frac{1}{2}\theta$$

The compressible generalization of the doublet is therefore

$$\psi_{\frac{1}{2}} = -Q_{\frac{1}{2}} \cos \frac{1}{2} \theta$$

(3) Consider the compressible generalization of the source. The complex velocity potential for a unit source at the origin is

$$\Omega = \log z$$

The reflected-velocity vector is

$$\frac{d\Omega}{dz} = \frac{1}{z}$$
$$= e^{-iw}$$

Hence

$$z=e^{iw}$$

and

$$\Omega = iw$$

The velocity potential for the incompressible source is

$$\phi = -\log q$$

The compressible generalization of the source is then given by

$$\phi_0 = -P_0$$

(4) Consider the compressible generalization of a point vortex. The complex velocity potential for a vortex of unit strength at the origin is

$$\Omega = -i \log z$$

The reflected-velocity vector is

$$\frac{d\Omega}{dz} = -\frac{i}{z}$$
$$= e^{-iw}$$

Hence

$$z = -ie^{iw}$$

and, except for an additive constant,

$$\Omega = w$$

The stream function for the incompressible vortex is

$$\psi = \log q$$

The compressible generalization of the vortex is then given by

$$\psi_0 = Q_0$$

TRANSFORMATION FROM THE HODOGRAPH TO THE PHYSICAL VARIABLES

Given the velocity potential ϕ and the stream function ψ in terms of the hodograph variables θ and q, it is possible to express the coordinates x and y of the physical plane in terms of θ and q.

From the basic flow equations

$$\frac{\partial \phi}{\partial x} = \frac{\rho_0}{\rho} \frac{\partial \psi}{\partial y}$$
$$\frac{\partial \phi}{\partial y} = -\frac{\rho_0}{\rho} \frac{\partial \psi}{\partial x}$$

it follows (see equation (6) of reference 1) that

$$dz = \frac{1}{q} e^{i\theta} \left(d\phi + i \frac{\rho_0}{\rho} d\psi \right)$$

The real and imaginary parts of this equation yield

$$dx = \frac{1}{q} \left[\left(\frac{\partial \phi}{\partial q} \cos \theta - \frac{\rho_0}{\rho} \frac{\partial \psi}{\partial q} \sin \theta \right) dq + \left(\frac{\partial \phi}{\partial \theta} \cos \theta - \frac{\rho_0}{\rho} \frac{\partial \psi}{\partial \theta} \sin \theta \right) d\theta \right]$$

$$dy = \frac{1}{q} \left[\left(\frac{\partial \phi}{\partial q} \sin \theta + \frac{\rho_0}{\rho} \frac{\partial \psi}{\partial q} \cos \theta \right) dq + \left(\frac{\partial \phi}{\partial \theta} \sin \theta + \frac{\rho_0}{\rho} \frac{\partial \psi}{\partial \theta} \cos \theta \right) d\theta \right]$$

$$(47)$$

Equations (47) relate the differential line elements in the physical xy-plane and the hodograph θq -plane. When expressions for ϕ and ψ as functions of θ and q are known for a given flow, the integrals of equations (47) are the equations of transformation of the θ,q coordinates to the x,y coordinates. It may be remarked that the hodograph flow equations (1) are the integrability conditions for the differential equations (47). The right-hand sides of equations (47) are therefore perfect differentials.

Consider one set of particular solutions from equations (4)

$$\phi = P_{k}(q) \cos k\theta$$

$$\psi = -Q_{k}(q) \sin k\theta$$

where $k=\pm 1$ and k=0 are excluded. By the use of equations (5), it can easily be verified that

$$x_{k} = \frac{k}{2} \left[\left(\frac{P_{k}}{q} - \frac{\rho_{0}}{\rho q} Q_{k} \right) \frac{\cos(k+1)\theta}{k+1} + \left(\frac{P_{k}}{q} + \frac{\rho_{0}}{\rho q} Q_{k} \right) \frac{\cos(k-1)\theta}{k-1} \right] + \text{Constant}$$

$$y_{k} = \frac{k}{2} \left[\left(\frac{P_{k}}{q} - \frac{\rho_{0}}{\rho q} Q_{k} \right) \frac{\sin(k+1)\theta}{k+1} - \left(\frac{P_{k}}{q} + \frac{\rho_{0}}{\rho q} Q_{k} \right) \frac{\sin(k-1)\theta}{k-1} \right] + \text{Constant}$$

$$(48)$$

The equations of transformation corresponding to the other set of particular solutions from equations (4) are obtained by replacing in equations (48) the cosine by the sine and the sine by the negative cosine.

The excluded cases k=0 and $k=\pm 1$ are now treated. For k=0, one set of particular solutions corresponds to a source and is

$$\phi_0 = -P_0$$

$$\psi_0 = \theta$$

Equations (47) then yield

$$x = \frac{\rho_0}{\rho q} \cos \theta$$

$$y = \frac{\rho_0}{\rho q} \sin \theta$$

The other set of particular solutions corresponds to a vortex and is

$$\phi_0 = \theta$$

$$\psi_0 = Q_0$$

Equations (47) then yield

$$x=\frac{1}{q}\sin\theta$$

$$y = -\frac{1}{q}\cos\theta$$

For k=1 with

$$\phi_1 = P_1 \cos \theta$$

$$\psi_1 = -Q_1 \sin \theta$$

equations (47) yield

$$x_{1} = \frac{1}{4} \left(\frac{P_{1}}{q} - \frac{\rho_{0}}{\rho q} Q_{1} \right) \cos 2\theta + \frac{1}{2} \int \left(\frac{1}{q} \frac{dP_{1}}{dq} + \frac{\rho_{0}}{\rho q} \frac{dQ_{1}}{dq} \right) dq$$

$$y_{1} = \frac{1}{4} \left(\frac{P_{1}}{q} - \frac{\rho_{0}}{\rho q} Q_{1} \right) \sin 2\theta - \frac{1}{2} \left(\frac{P_{1}}{q} + \frac{\rho_{0}Q_{1}}{\rho q} \right) \theta$$

With the use of equations (15) and (5),

$$x_{1} = \frac{1}{2} \left[1 - \frac{1 - (1 - \tau)^{\beta + 1}}{(\beta + 1)\tau(1 - \tau)^{\beta}} \right] \cos 2\theta + \log q$$

$$- \frac{\beta}{\beta + 1} g(\tau) - \frac{1}{2} \frac{2\beta + 1}{\beta + 1} \left[\frac{1}{(1 - \tau)^{\beta}} - 1 \right]$$

$$y_{1} = \frac{1}{2} \left[1 - \frac{1 - (1 - \tau)^{\beta + 1}}{(\beta + 1)\tau(1 - \tau)^{\beta}} \right] \sin 2\theta - \theta$$

$$(49)$$

where $g(\tau)=g_0(\tau)$ by equation (39) and is evaluated in part I (reference 1).

For k=1 with

$$\phi_1 = P_1 \sin \theta$$

$$\psi_1 = Q_1 \cos \theta$$

$$x_{1} = \frac{1}{2} \left[1 - \frac{1 - (1 - \tau)^{\beta + 1}}{(\beta + 1)\tau(1 - \tau)^{\beta}} \right] \sin 2\theta + \theta$$

$$y_{1} = \frac{1}{2} \left[1 - \frac{1 - (1 - \tau)^{\beta + 1}}{(\beta + 1)\tau(1 - \tau)^{\beta}} \right] \cos 2\theta + \log q$$

$$- \frac{\beta}{\beta + 1} g(\tau) - \frac{1}{2} \frac{2\beta + 1}{\beta + 1} \left[\frac{1}{(1 - \tau)^{\beta}} - 1 \right]$$
(50)

For k = -1 with

$$\phi_{-1}=P_{-1}\cos\theta$$

$$\psi_{-1} = Q_{-1} \sin \theta$$

equations (47) yield

$$\begin{split} x_{-1} &= \frac{1}{4} \left(\frac{P_{-1}}{q} + \frac{\rho_0 Q_{-1}}{\rho q} \right) \cos 2\theta + \frac{1}{2} \int \frac{1}{q} \frac{dP_{-1}}{dq} - \frac{\rho_0}{\rho q} \frac{dQ_{-1}}{dq} \right) dq \\ y_{-1} &= \frac{1}{4} \left(\frac{P_{-1}}{q} + \frac{\rho_0 Q_{-1}}{\rho q} \right) \sin 2\theta - \frac{1}{2} \left(\frac{P_{-1}}{q} - \frac{\rho_0}{\rho q} Q_{-1} \right) \theta \end{split}$$

With the use of equations (16) and (5),

$$x_{-1} = \frac{1}{4q^{2}} \left[\frac{3\beta + 2}{\beta + 1} \frac{1}{(1 - \tau)^{\beta}} - \frac{\beta}{\beta + 1} (1 + \beta \tau) \right] \cos 2\theta$$

$$+ \frac{1}{4a_{0}^{2}} \log q + \frac{3\beta + 2}{4(\beta + 1)a_{0}^{2}} g(\tau)$$

$$+ \frac{3\beta + 2}{8(\beta + 1)} \frac{2\beta + 1}{\beta a_{0}^{2}} \left[\frac{1}{(1 - \tau)^{\beta}} - 1 \right]$$

$$y_{-1} = \frac{1}{4q^{2}} \left[\frac{3\beta + 2}{\beta + 1} \frac{1}{(1 - \tau)^{\beta}} - \frac{\beta}{\beta + 1} (1 + \beta \tau) \right] \sin 2\theta + \frac{1}{4a_{0}^{2}} \theta$$
For $k = -1$ with

 $\phi_{-1} = -P_{-1}\sin\theta$

$$\psi_{-1} = Q_{-1} \cos \theta$$

$$x_{-1} = \frac{1}{4q^2} \left[\frac{3\beta + 2}{\beta + 1} \frac{1}{(1 - \tau)^{\beta}} - \frac{\beta}{\beta + 1} (1 + \beta \tau) \right] \sin 2\theta$$

$$- \frac{1}{4a_0^2} \theta$$

$$y_{-1} = -\frac{1}{4q^2} \left[\frac{3\beta + 2}{\beta + 1} \frac{1}{(1 - \tau)^{\beta}} - \frac{\beta}{\beta + 1} (1 + \beta \tau) \right] \cos 2\theta$$

$$+ \frac{1}{4a_0^2} \log q + \frac{3\beta + 2}{4(\beta + 1)a_0^2} g(\tau)$$

$$+ \frac{3\beta + 2}{8(\beta + 1)} \frac{2\beta + 1}{\beta a_0^2} \left[\frac{1}{(1 - \tau)^{\beta}} - 1 \right]$$
(52)

Ringleb (reference 2) gives an example of the flow of a compressible fluid around a semi-infinite line. An examination of Ringleb's stream function $\psi = \frac{1}{q} \sin \theta$ shows that it is a linear combination of ψ_1 and ψ_{-1} ; that is,

$$\psi = \left(-\frac{1}{4a_0^2}Q_1 + Q_{-1}\right)\sin\theta$$

In fact, all the external angle flows $(1 \le -k < \infty)$ are non-unique; for, in view of the discussion preceding equation (11), a general form of ψ_{-k} is

$$\psi_{-k} = q^{-k} [A \tau^k Y_k(\tau) + Y_{-k}(\tau)] \sin k\theta$$

where A is an arbitrary constant.

or

OBSERVATIONS ON LIMIT LINES

In the present section there are reviewed briefly certain conditions, discussed by Tollmien (reference 9) and Ringleb (reference 10), with regard to possible limitations on the potential flow of an adiabatic compressible fluid.

Consider the family of streamlines

$$\psi(\theta, q) = \text{Constant}$$

Then along a streamline

$$d\psi = \frac{\partial \psi}{\partial \theta} d\theta + \frac{\partial \psi}{\partial q} dq = 0$$

and, from equations (47), the line elements along a streamline are

$$dx = \frac{\rho_0}{\rho} \left[\frac{1}{q^2} (M^2 - 1) \left(\frac{\partial \psi}{\partial \theta} \right)^2 - \left(\frac{\partial \psi}{\partial q} \right)^2 \right] \frac{\cos \theta}{\partial \psi / \partial \theta} dq$$

$$dy = \frac{\rho_0}{\rho} \left[\frac{1}{q^2} (M^2 - 1) \left(\frac{\partial \psi}{\partial \theta} \right)^2 - \left(\frac{\partial \psi}{\partial q} \right)^2 \right] \frac{\sin \theta}{\partial \psi / \partial \theta} dq$$
(53)

Singular points along a streamline are characterized by the vanishing of the common factor of equations (53):

$$\left(\frac{\partial\psi}{\partial q}\right)^{2} - \frac{1}{q^{2}} \left(M^{2} - 1\right) \left(\frac{\partial\psi}{\partial\theta}\right)^{2} = 0 \tag{54}$$

(Stagnation points at which $\frac{\partial \psi}{\partial \theta}$ and $\frac{\partial \psi}{\partial q}$ vanish, the vortex for which $\frac{\partial \psi}{\partial \theta} = 0$ and the source for which $\frac{\partial \psi}{\partial q} = 0$, are excluded from this discussion.) Observe now from equations (47) that the Jacobian of the transformation from the hodograph variables θ and q to the physical-plane variables x and y is given by

$$J\left(\frac{x,y}{\theta,q}\right) = \frac{\rho_0}{\rho q^2} \left(\frac{\partial \phi}{\partial \theta} \frac{\partial \psi}{\partial q} - \frac{\partial \phi}{\partial q} \frac{\partial \psi}{\partial \theta}\right)$$
$$= \frac{1}{q} \left(\frac{\rho_0}{\rho}\right)^2 \left[\left(\frac{\partial \psi}{\partial q}\right)^2 - \frac{1}{q^2} \left(M^2 - 1\right) \left(\frac{\partial \psi}{\partial \theta}\right)^2 \right]$$
(55)

Thus, the vanishing of the Jacobian is equivalent to the condition for the existence of a singular locus for the family of streamlines

$$\psi(\theta,q) = \text{Constant}$$

This singular locus consists of points at which the streamlines undergo an abrupt change of curvature and means, physically, that the acceleration $q\frac{dq}{ds}$ of a fluid particle is infinite at such points.

Both Ringleb and Tollmien have shown that the singular locus for the streamlines is also the envelope of the Mach lines in the plane of flow. The Mach lines are related to the streamlines in such a way that the component of the fluid velocity normal to a Mach line is equal to the local velocity of sound. The Mach lines are identical with the so-called characteristic curves of the second-order partial differential equations for ϕ and ψ and are the integral curves of the

ordinary differential equation

$$d\theta^{2} - \frac{1}{q^{2}} (M^{2} - 1) dq^{2} = 0$$

$$d\theta = \pm \frac{1}{q} \sqrt{M^{2} - 1} dq$$
(56)

The real solutions of this differential equation interpreted in the physical xy-plane yield the Mach lines for a given flow. The solution of equation (56) is

$$\theta - \theta_0 = \pm \left[\frac{1}{\sqrt{\tau_s}} \tan^{-1}(\sqrt{\tau_s} \sqrt{M^2 - 1}) - \tan^{-1} \sqrt{M^2 - 1} \right]$$
 (57)

where $\tau_s = \frac{\gamma - 1}{\gamma + 1}$ and where θ_0 assumes the values of θ along the M=1 line for a given flow.

It is recalled that the function

$$H = \log q + h(\tau)$$

introduced in part I (reference 1) in connection with the geometric-mean type of velocity correction formula is a solution of the differential equation

$$dH = \pm \frac{\sqrt{1 - M^2}}{q} dq$$

in the subsonic range. Observe that a continuation of the function H into the supersonic range is given by equation (56) as

$$d\theta = \pm \frac{\sqrt{M^2 - 1}}{q} \, dq$$

In the supersonic range, the function $H=\theta-\theta_0$ can thus be interpreted as the hodograph of the Mach lines for a given flow.

The differential line elements dx and dy for the Mach lines in the physical plane are now given. From equations (47) and (56), the line elements along a Mach line for a given flow are

$$dx = \frac{\rho_0}{\rho q} (\pm \sqrt{M^2 - 1} \cos \theta - \sin \theta) \left(\frac{\partial \psi}{\partial q} \pm \frac{1}{q} \sqrt{M^2 - 1} \frac{\partial \psi}{\partial \theta} \right) dq$$

$$dy = \frac{\rho_0}{\rho q} (\pm \sqrt{M^2 - 1} \sin \theta + \cos \theta) \left(\frac{\partial \psi}{\partial q} \pm \frac{1}{q} \sqrt{M^2 - 1} \frac{\partial \psi}{\partial \theta} \right) dq$$
(58)

Singular points along a Mach line are characterized by the vanishing of the common factor of equations (58)

$$\frac{\partial \psi}{\partial g} \pm \frac{1}{g} \sqrt{M^2 - 1} \frac{\partial \psi}{\partial \theta} = 0 \tag{59}$$

Equation (59) represents in the plane of flow two possible singular loci or "limit lines" for the two families of Mach lines associated with the plus and minus signs in equation (56). Clearly, the two singular loci cannot occur simultaneously since the two conditions cannot be satisfied simultaneously. Observe that equation (59) is equivalent to the vanishing of the Jacobian given in equations (55). Thus, the vanishing of the Jacobian is not only the condition for the existence of a singular (cusp) locus for the streamlines but also the condition for the existence of a limit line (envelope) for the Mach lines.

The existence of a singular locus may be looked upon as being equivalent to the vanishing along a curve of the Jacobian $J\left(\frac{x_iy}{\theta,q}\right)$ of the transformation from the hodograph-plane variables θ and q to the physical-plane variables x and y. It is remarked that singular solutions exist for which the Jacobian $J\left(\frac{\theta,q}{x,y}\right)$ of the transformation from the physical-plane variables x and y to the hodograph-plane variables θ and q vanishes identically in a region of the physical plane. In this case, as Tollmien pointed out, θ and q are no longer independent variables and the flow cannot be described in the hodograph plane. Examples of these "missed flows" are the solutions of Meyer (reference 11) for supersonic flow inside and outside sharp angles.

It is of special interest to apply the condition for the vanishing of the Jacobian to the particular solutions ϕ_k and ψ_k treated in the early part of this paper. The expression for the Jacobian for a particular solution

$$\phi_{k} = P_{k} \cos k\theta$$

$$\psi_{k} = -Q_{k} \sin k\theta$$

is, with the use of equations (5), for $k \neq 0$,

$$J = \frac{\rho_0}{\rho q^2} \left(\frac{\partial \phi}{\partial \theta} \frac{\partial \psi}{\partial q} - \frac{\partial \phi}{\partial q} \frac{\partial \psi}{\partial \theta} \right)$$

$$= \frac{k^2}{q^3} \left[P_k^2 \sin^2 k\theta + \left(\frac{\rho_0}{\rho} \right)^2 (1 - M^2) Q_k^2 \cos^2 k\theta \right]$$
(60)

Clearly, this expression for J is positive in the subsonic range M < 1. At the sonic value M = 1, $P_{k} \neq 0$ (see table following equation (23)) and J is again positive. At the first zero of P_{k} in the supersonic range M > 1, $Q_{k} \neq 0$; hence, J is negative. The values of M, for all the pairs of values θ , M for which the Jacobian J vanishes, therefore lie between M = 1 and the value of M at the first zero of P_{k} (or S_{k}) in the supersonic range.

By means of the relation

$$P_{\mathbf{k}} = \frac{\rho_0}{\rho} Q_{\mathbf{k}} S_{\mathbf{k}}$$

the vanishing of the Jacobian yields

$$\cot k\theta = \mp \frac{S_k}{\sqrt{M^2 - 1}} \tag{61}$$

Equation (61) is the relation for pairs of values θ , M, which interpreted in the physical xy-plane constitute the limit line for the particular flow ϕ_k , ψ_k . The values of M that satisfy equation (61) accordingly lie between M=1 and the value of M at the first zero of S_k in the supersonic range.

This paper is closed with the following remarks on limiting values of M in connection with the use of velocity correction

formulas. The limiting local values of M in the case of uniform flow past a prescribed boundary, in general, depend on shape parameters. The use of a velocity correction formula, however, yields a constant limiting value of M that depends only on the particular correction formula used. The geometric-mean correction formula yields the value M=1; the approximation of Temple and Yarwood yields M=1.35; and the arithmetic-mean correction formula given in part I (reference 1), which is based on a linear combination of a source (limiting value M=1) and a vortex (limiting value $M=\infty$) or a spiral flow, yields the value M=1.15.

LANGLEY MEMORIAL AERONAUTICAL LABORATORY, NATIONAL ADVISORY COMMITTEE FOR AERONAUTICS, LANGLEY FIELD, VA., September 29, 1944.

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 - This reference, which appeared after the present paper was submitted for publication, contains graphical flow patterns associated with the particular solutions of index $k=\pm\frac{1}{2},\pm\frac{3}{2}$, and \pm 2.

ON THE FLOW OF A COMPRESSIBLE FLUID BY THE HODOGRAPH METHOD-II

TABLE 1.—THE FUNCTIONS Y_k FOR SEVERAL VALUES OF THE INDEX k

М	τ	Y _{0,5}	Y_1	Y1.3	Y2	Y2.5	Yıs	Y ₆	Y_0,	Y-1	Y _{-1.5}	Y-2	Y-2,5	Y-1.5	Y-3
0.1 .2 .3 .4 .5 .55 .6 .05	0. 00200 .00794 .01768 .03101 .04762 .05705 .06716 .07702 .08925 .10112	0. 99875 . 99505 . 98902 . 98085 . 97078 . 96513 . 95911 . 95276 . 94613 . 93925	0. 99751 . 99012 . 97809 . 90184 . 94188 . 93071 . 91884 . 9036 . 89336 . 87991	0. 99626 . 98520 . 96724 . 94306 . 91353 . 89707 . 87966 . 86141 . 84247 . 82297	0. 99502 .98030 .95648 .92456 .88584 .86438 .84176 .8118 .79383 .76888	0. 99378 .97542 .94582 .9038 .85886 .83268 .80524 .77678 .74755 .71778	0. 99130 . 96572 . 92481 . 87096 . 80709 . 77240 . 78042 . 60954 . 66213 . 62455	0. 98759 . 95134 . 89414 . 82027 . 73491 . 63961 . 64344 . 59703 . 55092 . 50563	1. 00125 1. 00494 1. 01094 1. 01904 1. 02897 1. 03453 1. 04042 1. 04660 1. 05304 1. 05969	1, 00249 1, 00982 1, 02162 1, 03728 1, 05606 1, 06637 1, 07714 1, 08828 1, 09967 1, 11122	1.00371 1.01442 1.03089 1.05128 1.07340 1.08441 1.09502 1.10499 1.11410 1.12216	1, 00517 1, 02207 1, 08313 1, 10000 1, 16253 1, 19901 1, 23835 1, 27993 1, 32307 1, 36702	1. 00634 1. 02642 1. 06271 1. 11785 1. 19120 1. 23423 1. 28044 1. 32883 1. 37819 1. 42716	1. 00883 1. 03632 1. 03697 1. 16425 1. 27940 1. 35293 1. 43746 1. 53249 1. 63666 1. 74773	1. 01261 1. 05178 1. 12213 1. 22409 1. 41003 1. 53449 1. 69314 1. 89526 2. 15092 2. 47001
.8 .825 .85 .875 .9 .925 .95 .96 .88	.11348 .11982 .12626 .13279 .13941 .14612 .16290 .16563 .16113 .16667	. 93216 . 92855 . 92491 . 92122 . 91751 . 91378 . 91002 . 90851 . 90549 . 90246	.86609 .85907 .85198 .84485 .83766 .83045 .82320 .82030 .81448 .80866	.80303 .79294 .78278 .77257 .76232 .76205 .74176 .78765 .72942 .72121	.74352 .73074 .71791 .70506 .69220 .67936 .66654 .66143 .65122 .64106	. 68772 . 67264 . 65756 . 64251 . 62751 . 61257 . 59773 . 59182 . 58006 . 56838	. 58723 . 56857 . 55015 . 53192 . 51289 . 49610 . 47856 . 47163 . 45790 . 44436	.46159 .44016 .41917 .30867 .37868 .35923 .34034 .33294 .31844 .30432	1, 06851 1, 06997 1, 07347 1, 07698 1, 08052 1, 08407 1, 08763 1, 08905 1, 09191 1, 09477	1, 12285 1, 12866 1, 13446 1, 14024 1, 14598 1, 15168 1, 15734 1, 15958 1, 16405 1, 16847	1, 12901 1, 13195 1, 13454 1, 13678 1, 13856 1, 14017 1, 14132 1, 14167 1, 14220 1, 14249	1, 41099 1, 43274 1, 45421 1, 47529 1, 49591 1, 51597 1, 53540 1, 54297 1, 55770 1, 57203	1, 47429 1, 49670 1, 51810 1, 53830 1, 55714 1, 57444 1, 59006 1, 59580 1, 60636 1, 61565	1. 86253 1. 92011 1. 97707 2. 03280 2. 08667 2. 13801 2. 18615 2. 20436 2. 23874 2. 27013	2.88074 3.08469 3.32803 3.59058 3.87173 4.17044 4.48517 4.61510 4.88108 5.15401
1.02 1.04 1.06 1.08 1.10 1.12 1.15 1.18 1.20 1.25	.17224 .17785 .18349 .18915 .19485 .20056 .20917 .21782 .22360 .23810	.89942 .89638 .89334 .89029 .88725 .88421 .87966 .87512 .87211 .86462	.80283 .79701 .79119 .78538 .777379 .76515 .75655 .75085 .73673	.71301 .70483 .69667 .58865 .68046 .67241 .66042 .64854 .64069 .62182	. 63094 . 62088 . 61088 . 60094 . 59108 . 58129 . 56677 . 55245 . 54303 . 51991	. 55680 . 54531 . 53394 . 52267 . 51153 . 50052 . 48424 . 46828 . 45782 . 43234	.43103 .41792 .40502 .39235 .37992 .36773 .34990 .33263 .32143 .29456	. 29068 . 27724 . 26430 . 25175 . 23961 . 22786 . 21098 . 19499 . 18481 . 16102	1. 09763 1. 10048 1. 10333 1. 10618 1. 10902 1. 11185 1. 11608 1. 12028 1. 12306 1. 12995	1, 17285 1, 17718 1, 18147 1, 18570 1, 18987 1, 19399 1, 20006 1, 20599 1, 2087 1, 21927	1. 14254 1. 14236 1. 14194 1. 14129 1. 14042 1. 18933 1. 13728 1. 13475 1. 13282 1. 12712	1, 58576 1, 59891 1, 61145 1, 62337 1, 63462 1, 64520 1, 65975 1, 67269 1, 68040 1, 69640	1, 62360 1, 63016 1, 63828 1, 63891 1, 64102 1, 64157 1, 63943 1, 63367 1, 62782 1, 60612	2, 29819 2, 32258 2, 34300 2, 35914 2, 37071 2, 37746 2, 37799 2, 36639 2, 35161 2, 28904	5. 43233 5. 71424 5. 99777 6. 28077 6. 56092 6. 83579 7. 23249 7. 60241 7. 82954 9. 30880
1. 30 1. 35 1. 40 1. 45 1. 50 1. 60 1. 65 1. 70 1. 75	. 25262 . 26713 . 28161 . 29602 . 31034 . 32455 . 33862 . 35254 . 36629 . 37984	.85721 .84990 .84270 .83563 .82889 .82190 .81526 .80877 .80245 .70630	. 72283 . 70915 . 69576 . 68265 . 66385 . 66738 . 64524 . 63345 . 62200 . 61091	.60238 .58338 .56587 .54838 .53141 .51500 .49913 .48383 .46909 .45491	. 49748 . 47576 . 45480 . 43461 . 41521 . 39680 . 37879 . 36177 . 34552 . 33004	.40784 .38436 .36192 .34053 .32019 .30089 .28262 .26535 .24905 .23370	. 26929 . 24563 . 22354 . 20301 . 18396 . 16635 . 15012 . 18520 . 12151 . 10897	.13953 .12022 .10297 .08763 .07406 .06213 .05168 .04258 .03469 .02789	1. 13673 1. 14339 1. 14990 1. 16627 1. 16249 1. 16854 1. 17442 1. 18014 1. 18568 1. 19105	1, 22825 1, 23680 1, 24491 1, 25260 1, 25866 1, 26669 1, 27312 1, 27914 1, 28479 1, 29006	1. 12030 1. 11246 1. 10370 1. 09414 1. 08389 1. 07306 1. 06176 1. 06009 1. 03814 1. 02599	1. 70770 1. 71430 1. 71632 1. 71392 1. 70731 1. 69677 1. 68258 1. 66508 1. 64459 1. 62146	1. 57447 1. 53323 1. 48294 1. 42427 1. 35802 1. 22639 1. 12291 1. 03562 . 94546	2. 18883 2. 05067 1. 87586 1. 66476 1. 42162 1. 14948 .85252 .53530 .20267 14043	8. 62759 8. 74667 8. 63279 8. 26094 7. 61597 6. 69350 5. 50014 4. 05311 2. 37916 . 51304
1, 80 1, 85 1, 90 1, 95 2, 00	.39320 .40635 .41928 .43198 .44444	.79031 .78449 .77885 .77337 .76805	.60017 .58978 .57974 .57005 .56070	. 44128 . 42819 . 41564 . 40361 . 39209	. 31530 . 30129 . 28798 . 27535 . 26337	. 21926 . 20569 . 19296 . 18102 . 16984	.09753 .08710 .07761 .06900 .06119	.02206 .01709 .01288 .00934 .00637	1, 19625 1, 20128 1, 20614 1, 21083 1, 21535	1, 29499 1, 29957 1, 30384 1, 30781 1, 31150	1, 01373 1, 00144 . 98916 . 97697 . 96490	1, 59603 1, 56864 1, 53961 1, 50924 1, 47782	.85334 .76012 .66659 .57349 .48146	-, 48912 -, 83871 -1, 18479 -1, 52335 -1, 85078	-1, 50416 -3, 62711 -5, 80829 -7, 99978 -10, 15503

TABLE 2.—THE FUNCTIONS S_k FOR SEVERAL VALUES OF THE INDEX k

M	7	S ₀	S0.5	S_1	S _{1.5}	S ₂	S _{2.4}	Sij	Sı.	S∞
). 1	0.00200	0, 99502	0, 99501	0.99501	0.99500	0. 99500	0. 99500	0.99500	0.99500	0.99499
.2	.00794	. 98028	. 98018	. 98012	. 98007	. 98004	.98001	.97997	. 97994	. 97980
.3	.01768	. 95638	95592	95560	. 95537	. 95520	. 95507	.95487	. 95468	. 9539
.4	.03101	. 92427	92286	. 92189	.92118	. 92064	. 92022	91958	. 91896 . 87242	. 9165
. 5	.03101 .04762 .05705	. 88517	. 88187	. 95560 . 92189 . 87957	. 87788	87657	. 87553	.87397 .84723	,87242	. 8660
. 55	. 05705	. 86342	. 85971	. 85541	. 85295	. 85105	. 84953	. 84723	.84492	. 8351
.6	1 .06716)	. 84045	. 83396	. 82938	.82594	. 82326	.82110	.81784	. 81451	.8000
. 65	.07792 .08925	. 816 44	. 83396 . 80777	. 85541 . 82938 . 80158	. 79692	. 85105 . 82326 . 79325	.79028	.78575 .75092	. 78109	.7599
.7	.08925	.79158	.78028	.77215	. 76596	.76105	.75706	. 75092	.74454	.7141
.75	.10112	.76604	.75164	.74118	. 73315	. 72674	.98000 .98001 .95507 .92022 .87553 .84953 .82110 .79028 .76706 .72148	.71332	. 70473	. 6614
.8	.11348	.78999	.72202	.70881 .69214 .67517 .65791 .64038 .62259	. 69858	. 69035	.68355 .66371 .64330 .62231 .60075 .57862 .55893 .54669 .52795 .50886	. 67295	. 66153	. 6000
. 825	.11982	. 72683	.70688	. 69214	. 68067	. 67140	. 66371	.65161	. 63860	. 5651
. 85	. 11982 . 12626	.71381	.70688 .69155	. 67517	. 66236	. 65196 . 63203	64330	. 62959 . 60684	. 63860 . 61475 . 58995	. 5267 . 4841
. 875	13279	.70034	. 67605	. 65791	. 64365	. 63203	.62231	.00084	. 08995	4841
.9	.13941	.68704	. 66039	.64038	. 62457	.61162	.60075	. 58334 . 56910 . 53409	. 56419 . 53742	. 4358 . 3799
. 925	.14812	. 67374	. 64459	. 022259	.60512	. 59074 . 56941	.0/802	*90810	.50962	.3122
. 95	15290	.66044	.62868	, 60457	. 58532	.00941	. 00093	. 52387	. 49820	3000
.96	.15563	.65518	. 62229	. 59730 . 58265	. 57730	. 56075	. 04009	10000	. 47484	.2800 .1990
. 98	. 16113	. 64452	.60945	. 58205	. 56111	. 54321	.02790	. 50306 . 48174	45078	0.1880
1.00	. 15667	. 63394	. 59657	. 56787	. 54472	. 52539	. 50,550			, ,
1.02	17224	. 62339	. 58364 . 57068	. 55298 . 53796 . 52285 . 50763 . 49233 . 47695	. 52812	. 50729 . 48893 . 47030	.48941 .46962 .44947 .42897 .40813 .36895 .35454 .32138 .20888	. 45992 . 43758	. 42594	
1.02 1.04	. 17224 . 17785	. 62339 . 61289	. 57068	. 53796	. 51134	. 48893	. 46962	. 43758	. 40036	
1.06	18349	.60243	55768	. 52285	. 49436	.47030	. 44947	.41473	. 37399	
1.06 1.08 1.10	. 18915 . 19485 . 20056	. 59203	. 54468 . 53165	. 50763	. 47721	. 45140 . 48225	. 42897	. 39135	. 34681	
1.10	. 19485	. 58170	. 53165	. 49233	. 45990	. 43225	. 40813	. 36743	. 31879	
112	.20056	. 57143	. 51863	. 47695	.44241	.41285	. 38695	. 34297 . 30526	. 28989	
1, 15	.20917	. 55616	. 51863 . 49910	. 45374 . 43040	,41590	. 38330	.35454	. 30526	. 24482	
1.18	.20917 .21782	. 54108	47961	. 43040	38906	. 35321	.32138	. 28628 . 23958	. 19759	
1. 15 1. 18 1. 20	22360	. 53114	. 46665	. 41477	.37100	.41285 .38330 .35321 .33286	.20885	.23958	. 16482	 -
1. 25	. 23810	. 50670	. 43438	. 37554	. 32531	.28104	. 24110	. 17025	.07809	
1, 30	. 25282	. 48290	. 40241 . 37082 . 33969	. 33616	. 27895	. 22793	.18133 .11960	. 09712 . 02001	01622 11915	-
1. 35	. 26713	. 45980	.37082	. 29675	. 23203 . 18467	.17362 .11821	111900	02001	11918 23203	
1.40	. 28161	. 43742	. 33969	. 29675 . 25740 . 21823	18467	.11821	.00090	06128	23203 35857	
1.45	29602	. 41581	.30909 .27908 .24971	.21823	. 13698	.06181	.05595 00958 07688	14700 23739	49497	
1.50	.31034 .32455	. 39498	.27908	.17932	.08907	.00451	07688 14595	23739 33276	65017	
1. 55	. 32455	. 37495	.24971	.14076	.04105	05357	14595 21670	33276 43347	82614	
1.60	. 33862	. 35573	.22103 .19308 .16589	.10588	00698	11233	21070 28906	53992	-1.02840	
T 69	. 85254	.33731	19508	.06500 .02795	05491 10264	17166 23145	28606 36296	65256	-1.26488	
1.85 1.40 1.45 1.50 1.55 1.60 1.65 1.70 1.75	.38829	.31969	.13948	02795 00847	10204 15009	23145 29159	43834	77196	-1.54739	
	. 37984	.30287			1				!	
1. 80 1. 85 1. 90 1. 95	.39320 .40635	. 28682 . 27153	.11387 .08907	04421 07921	19716 24276	35197 41249	51511 59320	89874 -1. 03387	-1.89427 -2.33576	
1.80			.08907	07821 11343	24376 28982	47803	59320 67251	-1,17762	-2.92543	
1.90	.41928	. 25699 . 24317	.04194	11685 14685	33527	53348	75295	-1.33167	-3, 76819	
1.95 2.00	. 43198 . 44444	.23005	.01960	17942	38003	59375	83445	-1.49711	-5. 10125	
4, UU	. 11111	. 23000	1 .01800	1/094	00000	00070	00110	1. 20.11	0. 20120	

TABLE 2.—THE FUNCTIONS S_k FOR SEVERAL VALUES OF THE INDEX k—Concluded

М	т	80	S-0.1	84	8-1.5	S-3	S-2.5	S-3,5	S.,	S _{co}
0. 1 .2 .3 .4 .5 .55 .66 .65 .7	0.00200 .00794 .01768 .03101 .04762 .05705 .06718 .07792 .08925 .10112	0. 99502 . 98028 . 95638 . 92427 . 88517 . 86342 . 84045 . 81644 . 79158 . 76604	0. 99503 . 98043 . 98714 . 92656 . 89040 . 87082 . 85053 . 82977 . 80874 . 78764	0. 99505 .98074 .95862 .93093 .90022 .83452 .86899 .85386 .83938 .82572	0. 99511 . 98165 . 96292 . 94336 . 92750 . 92218 . 91911 . 91858 . 92077 . 92683	0. 99470 97674 94371 89696 84251 81515 78929 76602 74630 73089	0. 99487 . 97823 . 94794 . 90476 . 85489 . 83074 . 80916 . 79166 . 77959 . 77411	0. 99494 . 97802 . 94966 . 90341 . 84049 . 80524 . 77005 . 73743 . 70999 . 69027	0. 99497 . 97944 . 95172 . 90716 . 83602 . 78695 . 72839 . 66200 . 69148 . 52200	0. 99499 .97980 .95394 .91652 .86603 .83516 .80000 .76993 .71414 .66144
.8 .825 .85 .875 .9 .925 .95 .96 .98	.11348 .11982 .12626 .13279 .13941 .14612 .15290 .15563 .16113 .16667	. 73999 . 72683 . 71361 . 70034 . 68704 . 67374 . 66044 . 645513 . 64452 . 63394	.76666 .75625 .74594 .73573 .72564 .71568 .70586 .70198 .69430 .68673	.81304 .80710 .80145 .79610 .79104 .78630 .78186 .78018 .77696	.93381 .93890 .94470 .95122 .93844 .96635 .97493 .97855 .98609 .99402	.72037 .71707 .71513 .71456 .71639 .71763 .72127 .72311 .72747 .73272	.77615 .78022 .78643 .79485 .80553 .81852 .83887 .84067 .85545 .87180	. 68050 . 67994 . 68256 . 68855 . 69808 . 71182 . 72846 . 73644 . 75441 . 77513	. 45926 . 43205 . 40833 . 38855 . 37302 . 36202 . 35570 . 35452 . 35449 . 35761	.60000 .56513 .52678 .48412 .43589 .37997 .31225 .28000 .19900
1.02 1.04 1.06 1.08 1.10 1.12 1.15 1.18 1.20 1.25	.17224 .17785 .18349 .18915 .19485 .20056 .20917 .21782 .22360 .23810	.62339 .61289 .60243 .59203 .58170 .57143 .55616 .54108 .53114 .50670	.67927 .67193 .66472 .65763 .65068 .64386 .63388 .62421 .61794 .60290	.77113 .76851 .76610 .76388 .76186 .76003 .75765 .75568 .75459 .75263	1. 00235 1. 01106 1. 02012 1. 02954 1. 03930 1. 04938 1. 06507 1. 08141 1. 09284 1. 12176	. 78884 . 74582 . 76366 . 76234 . 77186 . 78218 . 79915 . 81787 . 83128 . 86797	.88974 .90928 .93046 .95329 .97780 1.00401 1.04659 1.09319 1.12656 1,21833	. 79870 . 82526 . 85493 . 88787 . 92424 . 96425 1. 03159 1. 10856 1. 16579 1. 33275	. 36389 . 37338 . 38608 . 40203 . 42123 . 44384 . 48414 . 53245 . 66933 . 67937	
1,30 1,35 1,40 1,45 1,50 1,55 1,60 1,65 1,70 1,75	. 25262 . 26713 . 28161 . 29602 . 31034 . 32455 . 33862 . 35254 . 36629 . 37984	.48290 .45980 .43742 .41581 .39498 .37495 .35573 .33731 .31969 .30287	. 58875 . 57549 . 56312 . 55161 . 54095 . 53111 . 52204 . 51373 . 50612 . 49919	.75170 .75173 .76264 .75433 .75676 .75982 .76346 .76759 .77214	1. 15220 1. 18372 1. 21609 1. 24906 1. 26242 1. 31595 1. 34945 1. 38273 1. 41560 1. 44790	. 90893 . 95389 1. 00255 1. 05464 1. 10986 1. 16794 1. 22861 1. 29160 1. 35685 1. 42349	1. 32274 1. 44086 1. 57409 1. 72424 1. 80364 2. 08535 2. 30340 2. 55316 2. 84192 3. 17976	1. 54142 1. 80566 2. 14809 2. 60776 3. 25805 4. 25443 5. 99252 9. 86167 26. 61701 —38. 80980	. 81850 . 99367 1. 21624 1. 50541 1. 88549 2. 45352 3. 32923 4. 93773 9. 01193 43. 87853	
1.80 1.85 1.90 1.95 2.00	. 39320 . 40635 . 41928 . 43198 . 44444	. 28682 . 27153 . 25699 . 24317 . 23005	. 49289 . 48719 . 48205 . 47743 . 47329	. 78228 . 78772 . 79340 . 79920 . 80510	1. 47949 1. 51022 1. 53998 1. 56866 1. 59617	1, 49187 1, 56155 1, 63226 1, 70378 1, 77585	3. 58098 4. 06658 4. 66846 5. 43767 6. 46116	-11, 12607 -6, 40028 -4, 41184 -3, 29536 -2, 56565	-15, 39152 -6, 42359 -3, 94403 -2, 74361 -2, 00955	

TABLE 3.—THE FUNCTIONS R_k FOR SEVERAL VALUES OF THE INDEX k

M	т	R_0	Ro.3	R_1	$R_{1.5}$	R_2	$R_{2.5}$	R _{3.5}	R_5	R _∞
0.1 .2 .3 .4 .5 .55 .66 .65 .7	0. 00200 . 00794 . 01768 . 03101 . 04762 . 05705 . 06716 . 07792 . 08925 . 10112	0. 99496 97932 95150 90883 84729 80783 76149 70734 64428 57112	0. 99496 .97941 .95197 .91022 .85047 .81227 .76742 .71493 .65361 .68206	0. 99497 97947 95228 91117 85269 81540 77166 72045 66050 59027	0. 99497 97952 95251 91187 85433 81775 77487 72467 66584 59674	0. 99497 . 97955 . 95268 . 91241 . 85561 . 81958 . 77740 . 72802 . 67012 . 60201	0. 99497 97958 95221 91283 85662 82104 77944 73076 67366 60639	0. 99498 . 97962 . 95301 . 91346 . 85815 . 82327 . 78255 . 73497 . 67917 . 61333	0. 99498 97968 95320 91408 85608 82552 78575 73935 68409 62080	0. 99499 97980 95394 91652 86603 83516 80000 75993 71414 66144
.8 .825 .85 .875 .9 .925 .95 .96 .98 1,00	.11348 .11982 .12626 .13279 .13941 .14612 .15290 .15563 .16113 .16667	. 48649 . 43941 . 38887 . 33466 . 27655 . 21429 . 14763 . 11967 . 06144	. 49860 . 45181 . 40127 . 34668 . 22771 . 22398 . 15509 . 12599 . 06498	.50789 .46143 .41101 .35624 .29670 .23189 .16127 .13126 .06797	.51533 .46921 .41896 .36413 .30421 .23859 .16658 .13580 .07057	.52147 .47568 .42564 .37083 .31065 .24440 .17123 .13981 .07290	. 52666 . 48119 . 43137 . 37662 . 31627 . 24952 . 17538 . 14341 . 07501	. 53496 . 49014 . 44076 . 38622 . 32571 . 25823 . 18255 . 14966 . 07872	. 54419 . 50012 . 45140 . 39728 . 33677 . 26864 . 19132 . 15737 . 08340	.60000 .56513 .62678 .48412 .43589 .37997 .31225 .28000 .19900
1. 02 1. 04 1. 06 1. 08 1. 10 1. 12 1. 15 1. 18 1. 20 1. 25	.17224 .17785 .18349 .18915 .19485 .20056 .20917 .21782 .22300 .23810	06481 13314 20517 28107 36101 44520 57986 72521 82840 1,11012	06922 14299 22163 30550 33499 49052 64616 81816 94290 -1. 29494	07306 15168 23640 32780 42654 53339 71076 91172 -1. 06083 -1. 49784	07650 15958 25002 34869 45663 77543 77543 -1. 108588 -1. 18598 -1. 72910	07964 16690 26281 36863 48583 61620 84139 -1, 11096 -1, 32187 -2, 00149	08255 17376 27499 38790 51454 65745 90962 -1. 22100 -1. 47231 -2. 33308	08784 18648 29803 42520 57154 74175 1. 05649 -1. 47365 -1. 83658 -3. 30395	09485 20382 33049 47980 65874 87758 -1. 31727 -1. 98696 -2. 66958 -7. 20339	
1,30 1,35 1,40 1,45 1,50 1,65 1,65 1,70 1,75	. 25262 . 26713 . 28161 . 29602 . 31034 . 32455 . 33862 . 35254 . 36629 . 37984	-1, 42886 -1, 78883 -2, 19467 -2, 65144 -3, 16468 -3, 74045 -4, 38535 -5, 10657 -5, 91193 -6, 80994	-1, 71465 -2, 21804 -2, 82609 -3, 56693 -4, 47904 -5, 61652 -7, 05782 -8, 92117 -11, 39331 -14, 78750	-2. 05258 -2. 77171 -3. 72953 -5. 05195 -6. 97078 -9. 96383 -14. 73354 -26. 49894 -67. 62261 243. 44556	-2. 47363 -3. 54472 -5. 19836 -8. 04849 -14. 03370 -34. 16602 223. 57482 31. 37072 18. 41330 13. 74179	-3. 02728 -4. 73743 -8. 12116 -17. 83792 -277. 06111 26. 18116 13. 88787 10. 03451 8. 16600 7. 07332	-3. 80519 -6. 87721 -17. 15880 115. 26579 16. 25833 9. 60956 7. 19905 5. 95902 5. 20712 4. 70523	-7. 10444 -41. 10040 15. 66493 7. 50025 5. 26566 4. 21470 3. 59884 3. 19031 2. 89627 2. 67177	42, 54915 6, 90320 4, 13736 3, 09196 2, 52540 2, 15713 1, 88831 1, 67494 1, 49421 1, 33289	
1, 80 1, 85 1, 90 1, 95 2, 00	. 39320 . 40635 . 41928 . 43198 . 44444	-7, 80982 -8, 92157 -10, 15601 -11, 52488 -13, 04075	-19. 67235 -27. 19842 -40. 09831 -66. 82960 -153. 05279	50. 67121 30. 58443 23. 00938 19. 08458 16. 72046	11, 36148 9, 93797 9, 00545 8, 35894 7, 89411	6, 36416 5, 87292 5, 51767 5, 25323 5, 05263	4. 34856 4. 08381 3. 88101 3. 72201 3. 59520	2, 49237 2, 34360 2, 21633 2, 10449 2, 00386	1. 18251 1. 03714 . 89218 . 74372 . 58809	

TABLE 3.—THE FUNCTIONS R_k FOR SEVERAL VALUES OF THE INDEX k—Concluded

	-					l				1
M	Ŧ	R_0	R-0.5	R-1	R-1.5	R-1	R-2,5	R-3.5	R-5	Rω
0. 1 . 2 . 3 . 4 . 5 . 6 . 65 . 7 . 75	0.00200 .00794 .01768 .03101 .04762 .05705 .06716 .07792 .08925 .10112	0. 99496 . 97632 . 95150 . 90882 . 84729 . 80783 . 76149 . 70734 . 64428 . 57112	0. 99495 97916 95075 90658 84232 80097 75247 69598 63061 55546	0. 99493 . 97885 . 94928 . 90233 . 83313 . 78856 . 73649 . 67634 . 60759 . 52984	0. 99487 97795 94504 89043 80662 75636 69632 62869 55388 47255	0. 99528 98287 96428 93649 89020 85567 81086 75389 68337 59859	0, 99510 .98137 .95998 .92842 .87731 .83961 .79094 .72948 .65419 .56516	0, 99503 .98057 .95824 .92981 .89234 .86620 .83111 .78313 .71832 .63381	0, 99501 .98016 .95616 .92597 .89711 .88633 .87865 .87235 .86225 .83812	0. 99499 . 97880 . 95394 . 91652 . 86603 . 83516 . 80000 . 75993 . 71414 . 66144
.8 .825 .85 .876 .9 .925 .95 .96 .98	.11848 .11982 .12626 .13279 .13941 .14612 .16290 .15563 .16113 .16067	. 48649 . 43941 . 38887 . 33466 . 27655 . 21429 . 14763 . 11967 . 06144	.46957 .42231 .37201 .31856 .26184 .20173 .13813 .11168 .05704	. 44278 . 39570 . 34625 . 29441 . 24019 . 18361 . 12470 . 10049 . 05097	. 38552 . 34016 . 29374 . 24639 . 19824 . 14940 . 10001 . 08012 . 04016	. 49975 . 44539 . 38804 . 32800 . 26559 . 20118 . 13518 . 10842 . 05444	. 46383 . 40934 . 35286 . 29487 . 23587 . 17639 . 11693 . 09326 . 04629	. 52903 . 46971 . 40656 . 34039 . 27218 . 20297 . 13384 . 10646 . 05249	. 78387 . 73921 . 67059 . 60321 . 50936 . 38881 . 27411 . 22114 . 11171	.60000 .56513 .52678 .48412 .43589 .37097 .31225 .28000 .19900
1. 02 1. 04 1. 06 1. 08 1. 10 1. 12 1. 15 1. 18 1. 20 1. 25	.17224 .17785 .18349 .18915 .19485 .20056 .20917 .31782 .22360 .23810	06481 13314 20517 28107 38101 44520 57986 72521 82840 -1, 11012	, 05948 , 12144 , 18594 , 25303 , 32274 , 39512 , 50877 , 62863 , 71204 , 93300	, 05239, 10618, 16134, 21783, 27664, 33472, 42566, 51927, 58310, 74738	04031 08071 12116 16163 20206 24243 30280 36286 40269 50144	05468 10941 16400 21827 27207 32525 40355 47978 52930 64807	04541 08974 13284 17465 21477 25338 30814 35895 39057 46170	05058 09888 14457 18742 22721 26383 31262 35397 37743 42206	11102 21855 32014 41390 49850 57318 66613 73698 77284 82797	
1.30 1.35 1.40 1.45 1.50 1.55 1.60 1.65 1.70	.25262 .26713 .28161 .29602 .31034 .32455 .33862 .35254 .36629 .37984	-1.42886 -1.78883 -2.19467 -2.65144 -3.16468 -3.74045 -4.38535 -5.10657 -5.91193 -6.80994	-1, 17198 -1, 42922 -1, 70479 -1, 99868 -2, 31074 -2, 64071 -2, 98826 -3, 35295 -3, 73428 -4, 13169	91792 -1. 09415 -1. 27552 -1. 46156 -1. 65179 -1. 84583 -2. 04334 -2. 24405 -2. 44773 -2. 65423	59885 69484 78942 88266 97472 -1. 06577 -1. 15672 -1. 24573 -1. 33512 -1. 42447	75913 86226 95755 -1. 04538 -1. 12627 -1. 20083 -1. 26972 -1. 33361 -1. 39314 -1. 44890	52165 57084 60968 63941 66011 67255 67726 67726 64863	44764 45551 44691 42278 38366 32966 26032 17467 07101 . 05314	84300 82774 78932 73236 65946 57163 46858 34884 20972 04700	
1.80 1.85 1.90 1.95 2.00	. 39320 . 40635 . 41928 . 43198 . 44444	-7. 80982 -8. 92157 -10. 15601 -11. 52488 -13. 04075	-4. 54459 -4. 97236 -5. 41436 -5. 86997 -6. 33855	-2, 86343 -3, 07533 -3, 28965 -3, 50664 -3, 72624	-1.51404 -1.60407 -1.69483 -1.78656 -1.87950	-1. 50147 -1. 55135 -1. 59901 -1. 64488 -1. 68933	62553 69571 55907 51539 46431	. 20133 . 37850 . 59159 . 85044 1. 16930	. 14553 . 37713 . 66176 1. 02146 1. 49287	

TABLE 4.—THE FUNCTIONS f_k FOR SEVERAL VALUES OF THE INDEX k

M	т	fo	fo.s	fı	f1.5	f2	f2-5	fr:	fs.	ſω
0. 1 .2 .3 .4 .5 .55 .6 .65 .7	0.00200 .00794 .01768 .03101 .04762 .05705 .06716 .07792 .08925 .10112	-0.00250 00889 02196 03831 05847 06979 08186 09457 10787 12167	-0.00250 00991 02207 03867 05930 07099 08350 09678 11075 12534	-0.00250 00993 02215 03891 05987 07181 08464 09833 11277 12794	-0.00250 00994 02221 03908 06029 07241 08548 09946 11428 12989	-0.00250 00995 02225 03922 06061 07287 08613 10034 11545 13141	-0.00250 00996 02228 03932 06086 07324 08665 10104 11638 13263	-0.00250 00997 02233 03947 06123 07379 08742 10210 11780 13449	-0.00250 00998 02238 03962 06160 07433 08818 10316 11923 13639	-0.00250 01001 02256 04020 06306 07850 09133 10768 12541 14484
.8 .825 .85 .876 .9 .925 .95 .96 .98	.11348 .11982 .12626 .13279 .13941 .14612 .15290 .15563 .16113 .16667	13588 14313 15045 15785 16530 17281 18036 18339 18946 19556	14049 14825 15613 16410 17218 18034 18858 19189 19856 20526	, 14877, 15191, 16019, 16860, 17714, 18579, 19455, 19809, 20520, 21238	14624 15467 16327 17202 18093 18997 19915 20286 21033 21789	14818 15685 16571 17474 18394 19330 20283 20668 21446 22232	14975 15862 16769 17695 18640 19604 20585 20983 21785 22598	15210 16133 17073 18036 19021 20028 21056 21473 22318 23175	15462 16412 17389 18392 19421 20476 21556 21996 22887 23794	16605 17740 18927 20173 21487 22876 24353 24976 26292 27757
1.02 1.04 1.08 1.08 1.10 1.12 1.15 1.18 1.20 1.25	.17224 .17785 .18349 .18915 .19485 .20056 .20917 .21782 .22360 .23810	20166 20778 21391 22003 22616 23228 24144 25059 25665 27177	21201 21878 22558 23241 23925 24612 25644 26678 27368 29093	21961 22689 23422 24159 24900 25645 26769 27898 28655 30553	22551 23320 24096 24878 25696 27659 28869 29681 31727	23027 23831 24643 25463 26290 27125 28390 29669 30530 32705	23422 24258 25059 25952 26814 27685 29007 30348 31251 33542	24045 24928 25823 26731 27651 28583 30003 31450 33428 34922	24717 25657 26614 27588 28575 29581 31120 32697 33789 36524	
1.30 1.35 1.40 1.45 1.50 1.55 1.60 1.65 1.70	. 25262 . 26713 . 28161 . 29602 . 31034 . 32455 . 33862 . 35254 . 36629 . 37984	28673 30148 31604 33034 34438 35815 37163 38478 39763 41014	30814 32527 34229 36915 37582 39228 40851 42448 44017 45556	-, 32459 -, 34368 -, 36278 -, 38177 -, 40070 -, 41950 -, 43813 -, 45658 -, 47481 -, 49281	33792 35871 37959 40053 42148 44240 46325 48401 50464 52511	34910 37142 39395 41665 43949 46241 48539 50838 53135 55427	-, 35875 -, 38247 -, 40653 -, 43090 -, 45564 -, 50546 -, 50368 -, 55603 -, 58148	37485 40112 42804 45558 48372 51247 54180 57172 60223 63332	39389 42363 45467 48693 55572 55572 63129 67226 71589	
1,80 1,85 1,90 1,95 2,00	. 39320 . 40635 . 41928 . 43198 . 44444	42233 43418 44573 45690 46775	47066 48548 49989 51401 52779	51055 52800 54517 56203 57857	54539 56545 58529 60487 62418	57711 59984 62243 64485 66709	60700 63255 65811 68366 70916	66502 69734 73029 76391 79823	76278 81282 87038 93478 -1, 01119	

TABLE 4.—THE FUNCTIONS f_k FOR SEVERAL VALUES OF THE INDEX k—Concluded

М	τ	fo	f-0.s	<i>f</i> -1	f-1.3	f-1	f-1.5	f-1.5	f-s	fω
0. 1 .2 .3 .4 .5 .55 .6 .65 .7	0,00200 .00794 .01768 .03101 .04762 .05705 .06716 .07792 .08925 .10112	-0.00250 00989 02196 03831 05847 06979 08186 09457 10787 12167	-0.00250 00966 02176 03772 05712 06789 07925 09109 10336 11595	-0.00249 00977 02139 03660 05455 06426 07431 08459 09501 10546	0.00247 00954 02028 03334 04722 06052 06656 07203 07684	0. 00258 01091 02588 04766 07530 09075 10689 12340 13998 1,16632	-0.00253 01043 02433 04446 06998 08418 09888 11372 12831 14227	-0.00251 01019 02356 04345 07040 08636 10368 12197 14076 15952	-0,00251 -,01010 -,02305 -,04207 -,08564 -,10532 -,12787 -,15318 -,18084	-0.00250 01001 02256 04020 06306 07650 09133 10768 12641 14484
.8 .825 .85 .875 .9 .925 .95 .96 .98	.11348 .11982 .12626 .13279 .13941 .14612 .15290 .15563 .16113 .16667	13588 14313 15045 15785 16530 17281 18036 18339 18946 19556	12878 13526 14179 14832 15488 16144 16800 17061 17586 18109	11587 12103 12616 13123 13626 14122 14612 14906 15570	08089 08263 08415 08657 08657 08745 08813 08864 08881	17215 17979 18723 19443 20137 20803 21440 21686 22162 22619	15527 16131 16698 17227 17714 18156 18551 18959 19189	17770 18839 19475 20269 21016 21711 22347 22584 23026 23424	21022 22529 24048 25566 27074 28560 30016 30587 31707 32796	16605 17740 18927 20173 21487 24876 24976 26292 27767
1.02 1.04 1.06 1.08 1.10 1.12 1.15 1.18 1.20 1.25	.17224 .17785 .18349 .18915 .19485 .20056 .20917 .21782 .22360 .23810	20166 20778 21391 22003 22616 23228 24144 25059 25605 27177	18631 19149 19667 20183 20695 21205 21965 22716 23211 24435	15944 16312 16676 17033 17385 17730 18237 18730 19051 19825	08884 08873 08849 08811 08760 08576 08427 08314 07978	23053 23466 23857 24225 24571 24893 25333 25722 25952 26425	19386 19547 19673 19761 19813 19826 19774 19633 19490 18953	23778 24077 24327 24523 24663 24744 24750 24610 24431 23661	33847 34859 35828 36750 37623 38443 39572 40569 41158 42346	
1.30 1.35 1.40 1.45 1.50 1.65 1.65 1.70 1.75	. 25262 . 26713 . 28161 . 29602 . 31034 . 32455 . 33862 . 35254 . 36629 . 37984	28673 30148 31604 33034 34438 35815 37163 38478 39763 41014	25631 26800 27935 29040 30113 31151 32155 33127 34063 34967	20559 21253 21907 22522 23100 23641 24147 24619 25060 25469	07573 07105 06578 05998 05370 04701 03995 03258 02495 01711	26757 26950 27009 26939 26746 26436 26016 25494 24875 24166	18157 07095 15761 14146 12241 10033 07605 04637 01400 . 02244	22382 20519 17960 14562 10051 03980 04559 17855 . 45605	- 43099 - 43373 - 43111 - 42231 - 40605 - 38022 - 34095 - 27990 - 17335 - 13348	
1.80 1.85 1.90 1.95 2.00	.39320 .40635 .41928 .43198 .44444	42233 43418 44573 45690 46775	35838 36678 37485 38261 39006	25850 26203 26531 26835 27117	00909 00096 . 00727 . 01554 . 02382	23376 22510 21576 20580 19528	.06344 .10971 .16223 .22240 .29237			

TABLE 5.—THE FUNCTIONS g_k FOR SEVERAL VALUES OF THE INDEX k

	TUDDE	J.—11111	TONOI.	TOTAL YE	FUR SE	7 13101113		<u> </u>		
М	r	90	20.5	g ₁	g1.3	Ø2	92.5	Ø1.5	gs.	₽ ∞
0. 1 .2 .3 .4 .5 .55 .6 .65 .7	0. 00200 . 00794 . 01768 . 03101 . 04762 . 05705 . 06718 . 077792 . 08925 . 10112	-0. 00251 01013 02316 04208 06760 08309 10059 12023 14216 16657	-0. 00251 01010 02304 04174 06678 08194 09901 11814 13951 16327	-0.00251 01009 02298 04149 06622 08113 09791 11668 13763 16093	-0. 00250 01008 02291 04132 06581 08054 09709 11560 13621 15915	-0. 00250 01007 02287 04119 06549 08009 09646 11475 13511 15774	-0.00250 01006 02283 04108 06524 07973 09596 11407 13421 15660	-0.00250 -0.01006 -0.02278 -0.4093 -0.06487 -0.07919 -0.09521 -1.1305 -1.3287 -1.5486	-0.00250 01005 02274 04078 06451 07866 09445 11201 13149 15307	-0.00250 01001 02256 04020 06306 07650 09133 10768 12541 14484
.8 .825 .85 .875 .9 .925 .95 .96 .98	.11348 .11982 .12626 .13279 .13941 .14612 .15290 .15563 .16113 .16667	19363 20822 22354 23964 25652 27423 29280 30047 31624 33261	18967 20392 21893 23471 25131 26878 28715 29475 31045 32677	18681 20081 21566 23110 24747 28295 28051 30612 32243	18464 19841 21296 22829 24449 26158 27966 28717 30272 31901	18290 19652 21088 22605 24208 25903 27698 28446 29996 31622	18148 19496 20918 22421 24009 25692 27476 28220 29765 31389	17924 19255 20652 22130 23695 25367 27123 27861 29398 31019	17703 19001 20372 21823 23362 24997 26741 27472 28997 30614	16605 17740 18927 20173 21487 24876 24353 24976 26292 27767
1. 02 1. 04 1. 06 1. 08 1. 10 1. 12 1. 15 1. 18 1. 20 1. 25	.17224 .17785 .18349 .18915 .19485 .20058 .20917 .21782 .22360 .23810	34958 36718 38542 40432 42390 44417 47594 50938 53263 59432	34380 36150 37995 39915 41915 44001 47293 50798 53260 59892	33947 35728 37590 39539 41579 43718 47122 50785 53385 60509	33608 35397 37277 39251 41329 43518 47033 50858 53602 61269	33331 35129 37024 39023 41137 43377 47003 509945 53895 62176	33101 34907 36816 38838 40988 43278 47016 51187 54255 63251	32735 34554 36491 38559 40777 43168 47143 51708 55175 66083	32335 34174 36148 38282 40242 43163 47630 52846 57172 73925	
1. 30 1. 35 1. 40 1. 45 1. 50 1. 55 1. 60 1. 65 1. 70 1. 75	. 25262 . 26713 . 28161 . 29602 . 31034 . 32455 . 33802 . 3629 . 37984	66139 73409 81292 89817 99030 -1. 08984 -1. 19706 -1. 31258 -1. 43687 -1. 57037	-, 67231 -, 75539 -, 84801 -, 95235 -1, 07053 -1, 20528 -1, 36024 -1, 54028 -1, 75228 -2, 00636	68682 78158 89301 -1. 02644 -1. 19037 -1. 39926 -1. 64099 -2. 10316 -2. 91178	70377 81464 95446 -1 14078 -1 41442 -1 91708	- 72450 - 85838 -1. 04817 -1. 36976 -2. 67558	- 75054 - 92113 -1. 22912	83309 -1. 29668		
1.80 1.85 1.90 1.95 2.00	. 39320 . 40635 . 41928 . 43198 . 44444	-1, 71378 -1, 86763 -2, 03240 -2, 20875 -2, 39742	+2 31832 -2 71480 -3 24642 -4 02928 -5 45320							

TABLE 5.—THE FUNCTIONS g_k FOR SEVERAL VALUES OF THE INDEX k--Concluded

		·	1	1	1	ı	1		1	1
M	T	go	g-0.s	g −1	g−1.5	g-2	<i>g</i> −2,5	g-3.5	<i>g</i> -s	g to
0.1 .2 .3 .4 .5 .55 .6 .65 .7	0.00200 .00794 .01768 .03101 .04762 .05705 .06716 .07792 .08925 .10112	-0. 00251 01013 02316 04208 06760 08309 10059 12023 14216 16657	-0.00252 01018 02335 04265 06891 08494 10309 12347 14625 17158	-0. 00252 01025 02373 04377 07141 08840 10770 12941 15364 18049	-0. 00253 01048 02483 04697 08792 12016 14514 17282 20314	-0. 00242 00911 01922 03266 05060 06198 07548 09153 11053 13283	-0.00247 00959 02078 03592 05606 06875 08371 10139 12221 14646	-0.00249 00983 02155 03693 05560 06643 07869 09289 10968 12976	-0. 00250 00992 02207 03833 05730 06709 07670 08593 09490 10413	-0.00250 01001 02256 04020 06306 07650 09133 10768 12541 14484
.8 .825 .85 .876 .9 .925 .96 .98 1.00	.11348 .11982 .12626 .13279 .13941 .14612 .15290 .15563 .16113 .16667	19363 20822 22354 23964 27652 27423 29280 30047 31624 33261	19958 21463 23041 24691 26419 28222 30103 30877 32466 34107	21001 22579 24225 25939 27721 29571 31489 32275 33879 35524	23598 25330 27118 28959 30851 32792 34776 35582 37218 38868	17871 17803 18829 20448 22159 23958 25844 26622 28216 29859	17435 18968 20585 22290 24078 25942 27877 28670 30284 31934	15375 16734 18205 19784 21472 23262 25148 25927 27524 29169	11481 12126 12883 13783 14859 16137 17639 18305 19751 21345	16605177401892720173214872287624353249762629227757
1.02 1.04 1.06 1.08 1.10 1.12 1.15 1.18 1.20 1.25	.17224 .17785 .18349 .18915 .19485 .20056 .20917 .21782 .22360 .23810	34958 36718 38542 40432 42390 44417 47594 50938 53263 59432	37800 37545 39345 41201 43109 45073 48124 51299 53485 59200	37212 38940 40709 42518 44366 46253 49153 52134 54166 59390	40545 42244 43942 45697 47451 49217 51892 54590 £6403 60960	31548 33281 35055 36867 38713 40590 43458 46378 48348 53337	33616 35326 37061 38916 40°87 42371 45063 47764 49666 54046	30855 32577 34328 36102 37892 39693 42402 45103 46893 51292	23081 24947 26929 29009 31169 33390 36798 40247 42547 48211	
1.30 1.35 1.40 1.45 1.50 1.55 1.60 1.65 1.70	.25262 .26713 .28161 .29602 .31034 .32455 .33862 .36254 .36629 .37984	66139 73409 81292 89817 99030 -1. 08984 -1. 19706 -1. 31258 -1. 43687 -1. 57037	65267 71688 78453 85564 93010 -1. 00784 -1. 08871 -1. 17264 -1. 25946 -1. 34908	64811 70412 76175 82083 88119 94269 -1. 00515 -1. 06844 -1. 13241 -1. 19692	65547 70147 74745 79326 83880 88402 92881 97312 -1 01691 -1 06016	58380 63439 68479 73475 78403 83246 87889 92628 97146 -1. 01545	58462 62784 66982 71038 74937 78668 82224 85600 88795 91807	55543 59602 63435 67019 70338 73377 76129 78585 80737	53853 58785 63664 67963 71973 75592 78822 81663 84114 86170	
1, 80 1, 85 1, 90 1, 95 2, 00	.39320 .40635 .41928 .48198 .44444	-1.71378 -1.86763 -2.03240 -2.20875 -2.39742	-1. 44127 -1. 53594 -1. 63288 -1. 73193 -1. 83291	-1. 26187 -1. 32709 -1. 39260 -1. 45820 -1. 52385	-1, 10283 -1, 14492 -1, 18639 -1, 22728 -1, 26756	-1.05823 -1.09978 -1.14010 -1.17922 -1.21628	94637 97288 99750 -1. 02054 -1. 04173			

TABLE 6.—EXPONENTIALS OF THE FUNCTIONS f_k AND g_k FOR SEVERAL POSITIVE AND NEGATIVE VALUES OF THE INDEX k

М	e ^k	e10	e°°	e ^{f0.5}	80.1	e^{f_1}	e "1	e ^f 1.3	e ⁰ 1.3	e ^{f2}	e 02	e ^{f2.5}	e ⁰ 2.5	e ^{f3.5}	e ⁹ 3.5	e ^{fs}	e "3
0. 1 .2 .3 .4 .5 .55 .6 .65 .7	0.99750 ,99004 ,97769 .96060 .93889 .92635 .91271 .89792 .88213 .86616	0.99750 .99016 .97828 .96241 .94321 .93259 .92140 .90977 .89775 .88544	0.99749 .95992 .97711 .95879 .93463 .92026 .90430 .88671 .86748 .84656	0.99751 .99014 .97817 .96207 .94242 .93147 .91989 .90776 .89516 .88219	0.99749 .98995 .97722 .95912 .93540 .92133 .90573 .88857 .86978	0.99751 .99012 .97809 .96184 .94188 .93071 .91884 .90636 .80336 .87991	0.99750 .98996 .97730 .95936 .93593 .92207 .90673 .88987 .87142 .85135	0.99751 .99011 .97804 .96167 .94149 .93015 .91807 .90533 .89201 .87820	0. 99750 98997 97735 95952 93631 92262 90747 89083 87266 85287	0. 99751 .99010 .97800 .96154 .94119 .92972 .91747 .90453 .89097 .87686	0.99750 .98998 .97739 .95965 .93661 .92303 .90804 .89149 .87362 .85407	0.99751 .99009 .97796 .96144 .94095 .92938 .91700 .90390 .80013 .87579	0. 99750 .95999 .97743 .98975 .93684 .92337 .90850 .89220 .87441 .85505	0.99750 .99008 .97792 .96129 .94080 .9287 .91630 .90294 .88887 .87416	0.99750 .99000 .97747 .95990 .93719 .92388 .90918 .89311 .87558 .85654	0.99750 .99007 .97787 .96115 .94026 .92337 .91559 .90198 .88760 .87250	0. 99750 . 99000 . 97752 . 96004 . 93753 . 92438 . 90987 . 89403 . 87679 . 85807
.8 .825 .85 .875 .9 .925 .95 .96 .98	.84700 .83744 .82756 .81732 .80664 .79552 .78386 .77899 .70880 .75762	. 87295 . 86664 . 86032 . 85398 . 84764 . 84130 . 83497 . 83245 . 82741 . 82237	. 82397 . 81202 . 79968 . 78891 . 77374 . 76016 . 74617 . 74047 . 72888 . 71705	. 86893 . 80221 . 85545 . 84866 . 84183 . 83499 . 82814 . 82539 . 81991 . 81443	.82723 .81553 .80238 .79080 .77778 .76431 .75040 .74472 .73312 .72125	. 86609 . 85907 . 85198 . 84485 . 83768 . 83045 . 82320 . 82029 . 81448 . 80866	. 82960 . 81807 . 80609 . 70366 . 78077 . 76741 . 76356 . 74789 . 73630 . 72439	. 86395 . 85669 . 84936 . 84196 . 83440 . 82698 . 81943 . 81639 . 81031 . 80422	. 83140 . 82003 . 80819 . 79589 . 78310 . 76983 . 75604 . 75038 . 73881 . 72687	. 86228 . 85483 . 84730 . 83968 . 83199 . 82423 . 81642 . 81323 . 80698 . 80066	. 83285 . 82159 . 80987 . 79768 . 78499 . 77180 . 75807 . 75242 . 74085 . 72890	. 86092 . 85332 . 84£62 . 83782 . 82994 . 82198 . 81396 . 81073 . 80425 . 79773	. 83403 . 82287 . 81125 . 79915 . 78656 . 77343 . 75975 . 75412 . 74256 . 73060	. 85890 . 85102 . 84305 . 83497 . 82678 . 81850 . 81013 . 80676 . 70997 . 79315	. \$3591 . \$2485 . \$1341 . \$0148 . 78803 . 77603 . 76244 . 74684 . 74529 . 73331	. 85674 . 84864 . 84039 . 83200 . 82348 . 81484 . 80609 . 80255 . 79544 . 78825	. 83775 . 82695 . 81569 . 80394 . 79167 . 77882 . 76536 . 75978 . 74828 . 73628
м	e ^k	e ^f o	e ⁰ 0	e ^{f_0.5}	e -0.3	e ^{f_1}	e -1	e ^{f-1.5}	e ⁰ -1-3	e ^{f-2}	e ⁰⁻²	e ^{f_2,5}	e ⁰ -2.5	e ^{f_3,5}	e ⁹ -3.5	e ^{f_4}	e°-3
0, 1	0.99750	0.99750	0.99749	0.99750	0. 99749	0, 99751	0, 99749	0.99753	0, 99748	G. 99742	0. 99758	0.00=10		0.00740			0. 99751
.3 .4 .5 .55 .6 .65 .7	. 99004 . 97769 . 96060 . 93889 . 92635 . 91271 . 89792 . 88213 . 86516	.99016 .97828 .96241 .94321 .93259 .92140 .90977 .89775 .88544	.98992 .97711 .95879 .93463 .92026 .90430 .85671 .56748 .84656	. 99019 . 97847 . 90298 . 94448 . 93436 . 92381 . 91293 . 90180 . 89052	. 98088 . 97692 . 95824 . 93341 . 91856 . 90205 . 88385 . 86394 . 84233	. 99027 . 97884 . 96406 . 94691 . 93776 . 92838 . 91889 . 90936 . 89991	. 98981 . 97655 . 95717 . 93108 . 91£39 . 89790 . 87£61 . 85758 . 83486	.99050 .97\$92 .96721 .95388 .94741 .94128 .93561 .93050 .92604	. 08958 . 97548 . 95412 . 02463 . 90672 . 88678 . 86490 . 84129 . 81616	. 98914 . 97445 . 95346 . 92746 . 91325 . 89863 . 88391 . 86938 . 85529	. 99094 . 98097 . 98097 . 95085 . 93990 . 92729 . 91253 . 89536 . 87561	0. 99748 . 98962 . 97596 . 9£652 . 93241 . 91927 . 90585 . 89251 . 87958 . 86738	0, 997.53 .99045 .97943 .96472 .94548 .93356 .91970 .90358 .88496 .86376	0, 99749 98986 97671 95748 93202 91726 90151 88517 86870 85255	0. 99751 . 99022 . 97868 . 96375 . 94592 . 93573 . 92433 . 91130 . 89612 . 87831	0. 99750 .98395 .97722 .95881 .93359 .91793 .90004 .87997 .85798 .83457	.99012 .97817 .96240 .94432 .93511 .92617 .91765 .90947